



### 24-26 RAILWAY PARADE, WESTMEAD

### PEDESTRIAN WIND ENVIRONMENT STUDY

WD898-03F01(REV1)- WE REPORT

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Prepared for:

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#### DOCUMENT CONTROL

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#### **EXECUTIVE SUMMARY**

This report presents the results of a detailed investigation into the wind environment impact of the development located at 24-26 Railway Parade, Westmead. Testing was performed using Windtech's boundary layer wind tunnel, which has a 3.0m wide working section and has a fetch length of 14m. Measurements were made in the wind tunnel at selected critical outdoor locations within and around the development from 16 wind directions at 22.5 degree increments using a 1:300 scale detailed model. The effects of nearby buildings and land topography have been accounted for through the use of a proximity model, which represents an area with a radius of 375m.

Peak gust and mean wind speeds were measured at selected critical outdoor trafficable locations within and around the subject development. Wind velocity coefficients representing the local wind speeds are derived from the wind tunnel and are combined with a statistical model of the regional wind climate (which accounts for the directional strength and frequency of occurrence of the prevailing regional winds) to provide the equivalent full-scale wind speeds at the site. These wind speed measurements are compared with criteria for pedestrian comfort and safety, based on gust wind speeds which are representative of an annual recurrence, and Gust-Equivalent Mean (GEM) wind speeds which are representative of approximately a weekly recurrence.

The model was initially tested in the wind tunnel without the effects of any form of wind ameliorating devices such as screens, balustrades, etc. that are not already shown in the architectural drawings. The effect of vegetation was also excluded from this initial testing. If, however, the results of the study indicated that any area was exposed to strong winds, treatments have been tested in the wind tunnel to verify their effectiveness in wind mitigation. These treatments could be in the form of vegetation that is already proposed for the site, and/or additional trees, shrubs, screens, awnings, etc.

The initial tests results indicate that treatments are required for certain locations to achieve the desired wind speed criteria for pedestrian comfort and safety. The following treatments have been tested as part of the wind tunnel study to verify their effectiveness:

#### **Ground Level Areas**

- Inclusion of the proposed densely foliating trees with interlocking canopies along the southern perimeter (Railway Parade).
- Inclusion of an additional densely foliating tree capable of growing to a height of 3-4m with at least 3-4m wide canopy at the south-western corner of the development.
- Extension of the proposed eastern and southern awnings to connect at the southeastern corner.

• Glaze in the opening at the southern end of the atrium, for the section above the awning along Railway Parade.

#### Level 3 (Hotel Lobby)

- Inclusion of proposed landscaping for the Level 3 Terrace.
- Extension of the proposed densely foliating evergreen hedge at the north-eastern corner of the terrace space. The hedge needs to be capable of growing to a height of 1.5m.
- Make the proposed awning on Level 3 Terrace to be impermeable.

A comparative analysis of the wind directional plots for the various study points with and without treatments indicates that a revised treatment strategy is necessary to achieve the desired wind speed criteria for pedestrian comfort at the south-western and south-eastern corners of the subject development. To achieve the desired wind speed criteria, the following in-principle treatments, in addition to the tested treatments, are recommended for the Ground Level areas:

- Inclusion of 1.2m high portable operator-controlled screens at the south-western corner of the subject development if this area is to be used for seating such as for outdoor café seating. Wind conditions in this section of the building frontage currently satisfy the comfortable walking criterion without the portable screens.
- Extension of proposed southern awning towards the south-eastern corner of the subject development. The proposed extension to the southern awning will be sufficient to improve the wind conditions at the south-eastern corner.

It is expected that with the inclusion of the above in-principle recommendations, in addition to the tested treatments, wind conditions for all outdoor trafficable areas within and around the proposed development will be suitable for their intended uses.

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#### 1 WIND CLIMATE FOR THE SYDNEY REGION

Details of the wind climate of the Sydney region have been determined from a detailed statistical analysis of measured mean wind speed data from the meteorological observation station located at Kingsford Smith airport (Sydney Airport). The data has been collected from this station from 1995 to 2016, and corrected so that it represents winds over standard open terrain at a height of 10m above ground. The corrected data is summarised Table 1 for the weekly and annual return periods in the form of hourly means and the corresponding 3-second gust values. These directional wind speeds are also presented in Figure 1 (referenced as hourly mean wind speeds), as well as the directional frequency of occurrences for the region.

The data indicates that, for the weekly and annual return periods, the southerly winds are by far the most frequent winds for the Sydney region, and are also the strongest. The westerly winds occur most frequently during the winter season for the Sydney region, and although they are typically not as strong as the southerly winds, they are usually a cold wind and hence can be a cause for discomfort for outdoor areas. North-easterly winds occur most frequently occur during the warmer months of the year for the Sydney region, and hence are usually welcomed within outdoor areas since they are typically not as strong as the southerly not as strong as the southerly region.

	Reference Wind Speeds (m/s)					
Wind Direction	Weekly R	ecurrence	Annual R	ecurrence		
	Hourly Mean	3-second Gust	Hourly Mean	3-second Gust		
Ν	5.8	8.8	9.8	15.0		
NNE	9.4	14.3	12.5	19.0		
NE	9.1	13.8	11.9	18.2		
ENE	7.0	10.7	9.8	14.9		
E	5.9	9.0	9.2	14.0		
ESE	6.0	9.2	9.1	13.9		
SE	6.8	10.4	10.0	15.2		
SSE	8.5	12.9	12.1	18.5		
S	10.1	15.4	13.8	21.1		
SSW	9.8	14.9	13.9	21.2		
SW	7.0	10.7	11.8	18.1		
WSW	8.9	13.6	13.2	20.1		
W	9.3	14.2	14.0	21.3		
WNW	7.7	11.7	13.7	20.9		
NW	5.9	9.1	12.1	18.4		
NNW	5.3	8.1	10.3	15.7		

### Table 1: Directional Mean and Gust Wind Speeds for the Sydney Region (referenced to 10m height above ground in standard open terrain)

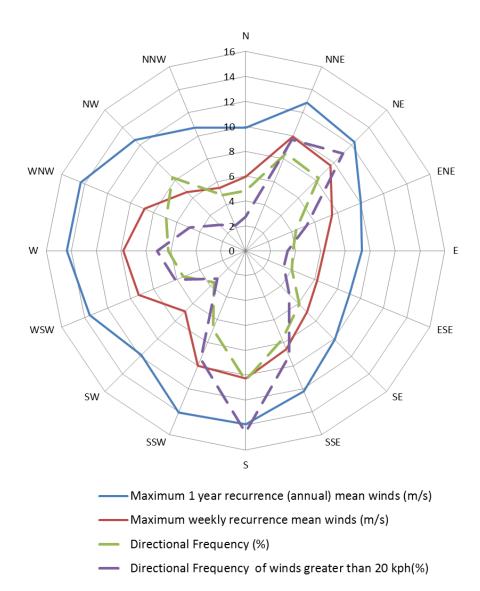


Figure 1: Directional Hourly Mean Wind Speeds, and Frequencies of Occurrence, for the Sydney Region (for the annual and weekly return periods, referenced to standard open terrain at a height of 10m above ground)

#### 2 THE WIND TUNNEL MODEL

Wind tunnel testing was undertaken to obtain accurate wind speed measurements at selected critical outdoor locations within and around the development using a 1:300 scale model. The study model incorporates all necessary architectural features on the development to ensure an accurate wind flow is achieved around the model. A proximity model has been constructed and represents the surrounding buildings and significant topographical effects within a radius of 375m, centred on the development site. Photographs of the wind tunnel model for the proposed scenario are presented in Figures 2a to 2f and for the existing scenario in Figures 2g to 2i on the following pages.

The model was tested in the wind tunnel without the effect of any forms of wind ameliorating devices such as screens, balustrades, etc. that are not already shown in the architectural drawings. The effect of vegetation was also excluded from the initial testing. If the results of the study indicate that any area is exposed to strong winds, treatments have been tested for those particular locations. These treatments could be in the form of vegetation that is already proposed for the site, and/or additional trees, shrubs, screens, awnings, etc. Existing wind conditions have also been tested for the critical trafficable outdoor locations at street level and these results have been compared against the results with the proposed development in-place.



Figure 2a: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the south)



Figure 2b: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the south-east)



Figure 2c: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the east)



Figure 2d: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the south-south-east)



Figure 2e: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the west)



Figure 2f: Photograph of the Wind Tunnel Model – Proposed Scenario (view from the east)



Figure 2g: Photograph of the Wind Tunnel Model – Existing Scenario (view from the south-east)

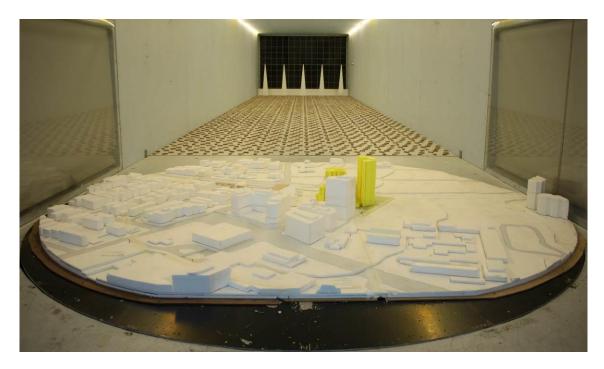


Figure 2h: Photograph of the Wind Tunnel Model – Existing Scenario (view from the north)



Figure 2i: Photograph of the Wind Tunnel Model – Existing Scenario (view from the south-east)

#### **3 BOUNDARY LAYER WIND FLOW MODEL**

Testing was performed using Windtech's boundary layer wind tunnel, which has a 3.0m wide working section and has a fetch length of 14m. The model was placed in the appropriate standard boundary layer wind flow for each of the prevailing wind directions for the wind tunnel testing. The type of wind flow used in a wind tunnel study is determined by a detailed analysis of the surrounding terrain types around the subject site. Details of the analysis of the surrounding terrain for this study are provided in the following pages of this report.

The roughness of the earth's surface has the effect of slowing down the prevailing wind near the ground. This effect is observed up to what is known as the *boundary layer height*, which can range between 500m to 3km above the earth's surface depending on the roughness of the surface (i.e. oceans, open farmland, dense urban cities, etc.). Within this range, the prevailing wind forms what is known as a *boundary layer wind profile*.

Various wind codes and standards classify various types of boundary layer wind flows depending on the surface roughness. However, it should be noted that the wind profile does not change instantly due to changes in the terrain roughness. It can take many kilometres (at least 100km) of a constant surface roughness for the boundary layer profile to achieve a state of equilibrium. Descriptions of the standard boundary layer profiles for various terrain types are summarised as follows (as per the definitions in AS/NZS1170.2:2011):

- **Terrain Category 1.0:** Extremely flat terrain. Examples include enclosed water bodies such as lakes, dams, rivers, bays, etc.
- **Terrain Category 1.5:** Relatively flat terrain. Examples include the open ocean, deserts, and very flat open plains.
- **Terrain Category 2.0:** Open terrain. Examples include grassy fields and plains and open farmland (without buildings or trees).
- **Terrain Category 2.5:** Relatively open terrain. Examples include farmland with scattered trees and buildings and very low-density suburban areas.
- **Terrain Category 3.0:** Suburban and forest terrain. Examples include suburban areas of towns and areas with dense vegetation such as forests, bushland, etc.
- **Terrain Category 3.5:** Relatively dense suburban terrain. Examples include centres of small cities, industrial parks, etc.
- **Terrain Category 4.0:** Dense urban terrain. Examples include CBD's of large cities with many high-rise towers, and areas with many closely-spaced mid-rise buildings.

For this study, the shape of the boundary layer wind flows over standard terrain types is defined as per ISO4354:2009. These are summarised in Table 2, referenced to the study reference height of 90m above ground.

# Table 2: Terrain and Height Multipliers, Turbulence Intensities, and CorrespondingRoughness Lengths, for the Standard ISO4354:2009 Boundary Layer Profiles(at the study reference height)

	Terrain	and Height Mult	ipliers	Turbulence Roughnes	
Terrain Category	$k_{\scriptscriptstyle tr,T=3600s}$ (hourly)	$k_{tr,T=600s}$ (10-minute)	$k_{tr,T=3s}$ (3-second)	Intensity $I_v$	Length (m) $\mathcal{Z}_{0,r}$
1.0	0.88	0.91	1.21	0.124	0.003
1.5	0.82	0.85	1.17	0.141	0.01
2.0	0.76	0.79	1.13	0.161	0.03
2.5	0.68	0.71	1.07	0.191	0.1
3.0	0.59	0.63	1.00	0.231	0.3
3.5	0.47	0.51	0.91	0.304	1
4.0	0.35	0.39	0.80	0.436	3

An analysis of the effect of changes in the upwind terrain roughness was carried out for each of the wind directions studied. This has been undertaken based on the method given in AS/NZS1170.2:2011, which uses a "fetch" length of 40 times the study reference height. However, it should be noted that this "fetch" commences *beyond* a "lag distance" area, which has a length of 20 times the study reference height (in accordance with AS/NZS1170.2:2011), so the actual "fetch" of terrain analysed is the area between 20 and 60 times the study reference height away from the site. An aerial image showing the surrounding terrain is presented in Figure 3 for a radius of 1.6km from the edge of the wind tunnel proximity model. The resulting mean and gust terrain and height multipliers at the site location are presented in Table 3, referenced to the study reference height.

For each of the 16 wind directions tested in this study, the approaching boundary layer wind profiles modelled in the wind tunnel matched the model scale and the overall surrounding terrain characteristics beyond the extent of the proximity model. Plots of the wind tunnel boundary layer wind profiles are presented in Appendix B of this report.

Wind Sector (degrees)	$k_{\scriptscriptstyle tr,T=3600s}$ (hourly mean)	$k_{\scriptscriptstyle tr,T=600s}$ (10-minute mean)	$k_{tr,T=3s}$ (3-second gust)
0	0.56	0.60	0.98
30	0.53	0.57	0.95
60	0.61	0.65	1.02
90	0.55	0.59	0.96
120	0.54	0.58	0.96
150	0.63	0.67	1.03
180	0.59	0.63	1.00
210	0.59	0.63	1.00
240	0.59	0.63	1.00
270	0.59	0.63	1.00
300	0.59	0.63	1.00
330	0.56	0.59	0.97

## Table 3: Terrain and Height Multipliers for Each Directional Sector(at the study reference height)

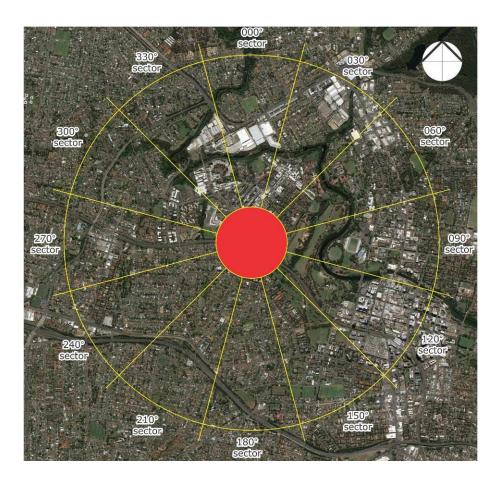


Figure 3: Aerial Image of the Surrounding Terrain (radius of 1.6km from the edge of the proximity model, which is coloured red)

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#### 4 ENVIRONMENTAL WIND SPEED CRITERIA

#### 4.1 Wind Effects on People

The acceptability of wind in any area is dependent upon its use. For example, people walking or window-shopping will tolerate higher wind speeds than those seated at an outdoor restaurant. Various other researchers, such as A.G. Davenport, T.V. Lawson, W.H. Melbourne, A.D. Penwarden, etc, have published criteria for pedestrian comfort for pedestrians in outdoor spaces for various types of activities. These are discussed in the following sub-sections of this report.

#### 4.1.1 A.D. Penwarden (1975) Criteria for Gust Wind Speeds

The following table developed by A.D. Penwarden (1975) is a modified version of the Beaufort scale, and describes the effects of various wind intensities on people. Note that the applicability column related to wind conditions occurring frequently (approximately once per week on average). Higher ranges of wind speeds can be tolerated for rarer events.

Type of Winds	Beaufort Number	Mean Wind Speed (m/s)	Effects
Calm, light air	1	0 - 1.5	Calm, no noticeable wind
Light breeze	2	1.6 - 3.3	Wind felt on face
Gentle breeze	3	3.4 - 5.4	Hair is disturbed, Clothing flaps
Moderate breeze	4	5.5 - 7.9	Raises dust, dry soil and loose paper - Hair disarranged
Fresh breeze	5	8.0 - 10.7	Force of wind felt on body
Strong breeze	6	10.8 - 13.8	Umbrellas used with difficulty, Hair blown straight, Difficult to walk steadily, Wind noise on ears unpleasant.
Near gale	7	13.9 - 17.1	Inconvenience felt when walking.
Gale	8	17.2 - 20.7	Generally impedes progress, Great difficulty with balance.
Strong gale	9	20.8 - 24.4	People blown over by gusts.

#### Table 4: Summary of Wind Effects on People (after A.D. Penwarden, 1975)

#### 4.1.2 A.G. Davenport (1972) Criteria for Mean Wind Speeds

A.G. Davenport (1972) had also determined a set of criteria in terms of the Beaufort Scale and for various return periods. The values presented in Table 5 below are based on a frequency of exceedance of approximately once per week (a probability of exceedance of 5%).

Classification	Activities	95 Percentile Maximum Mean (approximately once per week)
Walking Fast	Acceptable for walking, main public accessways.	7.5 m/s < $\overline{V}$ < 10.0 m/s
Strolling, Skating	Slow walking, etc.	5.5 m/s < $\overline{V}$ < 7.5 m/s
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	3.5 m/s < $\overline{V}$ < 5.5 m/s
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	$\overline{V}$ < 3.5 m/s

#### Table 5: Criteria by A.G. Davenport (1972)

#### 4.1.3 T.V. Lawson (1975) Criteria for Mean Wind Speeds

In 1973, T.V. Lawson quotes that A.D. Penwarden's Beaufort 4 wind speeds (as listed in Table 3) would be acceptable if it is not exceeded for more than 4% of the time; and a Beaufort 6 as being unacceptable if it is exceeded more than 2% of the time. Later, in 1975, T.V. Lawson presented a set of criteria very similar to those of A.G. Davenport's. These are presented in Tables 6 and 7.

#### Table 6: Safety Criteria by T.V. Lawson (1975)

Classification	Activities	Annual Maximum Mean
Safety (all weather areas)	Accessible by the general public.	15 m/s
Safety (fair weather areas)	Private outdoor areas (balconies, terraces, etc.)	20 m/s

#### Table 7: Comfort Criteria by T.V. Lawson (1975)

Classification	Activities	95 Percentile Maximum Mean (approximately once per week)	
Business Walking	Objective Walking from A to B.	8 m/s < $\overline{V}$ < 10m/s	
Pedestrian Walking	Slow walking, etc.	6 m/s < $\overline{V}$ < 8 m/s	
Short Exposure Activities	Pedestrian standing or sitting for short times.	4 m/s < $\overline{V}$ < 6 m/s	
Long Exposure Activities	Pedestrian sitting for a long duration.	$\overline{V}$ < 4 m/s	

#### 4.1.4 W.H. Melbourne (1978) Criteria for Gust Wind Speeds

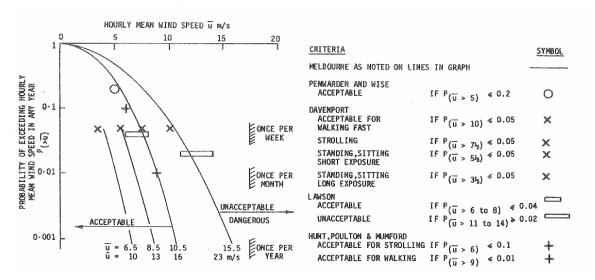
W.H. Melbourne (1978) introduced a set of criteria for the assessment of environmental wind conditions, which were developed for a temperature range of 10°C to 30°C and for people suitably dressed for outdoor conditions. These criteria are based on peak annual maximum gust wind speeds, and are outlined in Table 8 below. It should be noted that this criteria tends to be more conservative than criteria suggested by other researchers.

Classification	Human Activities	Annual Maximum Gust
Limit for safety	Completely unacceptable: people likely to get blown over.	$\hat{V}$ > 23m/s
Marginal	Unacceptable as main public accessways.	23 m/s > $\hat{V}$ > 16 m/s
Comfortable Walking	Acceptable for walking, main public accessways	16 m/s > $\hat{V}$ > 13 m/s
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	13 m/s > $\hat{V}$ > 10 m/s
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	10 m/s > $\hat{V}$

#### Table 8: Criteria by W.H. Melbourne (1978)

#### 4.2 Comparison of the Various Wind Speed Criteria

The criteria by W.H. Melbourne (1978) mentioned in Table 8, and criteria from other researchers, are compared on a probabilistic basis in Figure 4. This indicates that the criteria by W.H. Melbourne (1978) are quite conservative. This was also observed by A.W. Rofail (2007) when undertaking on-site remedial studies, who concluded that the criteria by W.H. Melbourne (1978) generally overstates the wind effects in a typical urban setting, which is caused by the assumption by W.H. Melbourne of a fixed 15% turbulence intensity for all areas. This value tends to be at the lower end of the range of turbulence intensities, and the A.W. Rofail (2007) study found that, in an urban setting, the range of the *minimum* turbulence intensities is typically in the range of 20% to 60%.



# Figure 4: Comparison of Various Mean and Gust Wind Environment Criteria, assuming 15% turbulence and a Gust Factor of 1.5 (after W.H. Melbourne, 1978)

#### 4.3 Wind Speed Criteria Used for This Study

For this study, the measured wind conditions for the various critical outdoor trafficable areas within and around the subject development are compared against two sets of criteria. For comfort, the A.G. Davenport (1972) criteria are used in conjunction with a maximum Gust-Equivalent Mean (GEM) wind speed (defined below), which are representative of approximately a weekly recurrence. The safety limit criterion by W.H Melbourne (1978) of 23m/s for the annual maximum peak gust wind speeds is also used. Note that the A.G. Davenport (1972) criteria, used in conjunction with a GEM wind speed (defined below), has proven over time, and through field observations, to be the most reliable indicator of pedestrian comfort (Rofail, 2007). Note also that the safety limit criterion by W.H Melbourne (1978) of 23m/s for annual maximum peak gust wind speeds is also applied to all areas.

The basic criteria for a range of outdoor activities are described as follows:

- **Short Exposure:** 5.5m/s maximum GEM wind speeds (representative of approximately a weekly recurrence).
- **Comfortable Walking:** 7.5m/s maximum GEM wind speeds (representative of approximately a weekly recurrence).
- **Safety Limit:** 23m/s annual maximum gust wind speeds.

Additionally, the existing wind conditions have also been tested as part of this study to determine the impact of the subject development. The results of the wind tunnel study are summarised in the following section, and presented in the form of directional plots attached in Appendix A of this report. Each study point has 2 plots; one comparing to the modified version of the A.G. Davenport (1972) criteria for the maximum GEM wind speeds (which are representative of approximately a weekly recurrence), and the other comparing to the W.H Melbourne (1978) for the annual maximum peak gust wind speeds.

#### Notes:

- The GEM is defined as the maximum of the mean wind speed and the gust wind speed divided by a gust factor of 1.85.
- The gust wind speed is defined as 3.0 standard deviations from the mean for a 3 second gust duration, or 3.4 standard deviations from the mean for a 0.5 second gust duration.
- Short Exposure applies typically to areas where short duration stationary activities are involved (less than 1 hour). This includes window shopping, waiting areas, etc.
- Comfortable Walking applies typically to areas used mainly for pedestrian thoroughfares. This also includes private swimming pools, communal areas, and private balconies and terraces.
- In all areas, the wind conditions are also checked against the safety limit.

#### 5.1 Measurement of the Velocity Coefficients

Testing was performed using Windtech's boundary layer wind tunnel facility, which has a 3.0m wide working section and has a fetch length of 14m. The test procedures followed for the wind tunnel testing performed for this study generally adhere to the guidelines set out in the Australasian Wind Engineering Society Quality Assurance Manual (AWES-QAM-1-2001), ASCE-7-10 (Chapter C31), and CTBUH (2013) guidelines.

The model of the subject development was setup within the wind tunnel, and the wind velocity measurements were monitored using Dantec hot-wire probe anemometers at selected critical outdoor locations at a full-scale height of approximately 1.5m above ground/slab level. The probe support for each study location was mounted such that the probe wire was vertical as much as possible, which ensures that the measured wind speeds are independent of wind direction along the horizontal plane. In addition, care was taken in the alignment of the probe wire and in avoiding wall-heating effects. Wind speed measurements are made in the wind tunnel for 16 wind directions, at 22.5° increments. The output from the hot-wire probes was obtained using a National Instruments 12-bit data acquisition card. A sample rate of 1,024Hz was used, which is more than acceptable for the given frequency band.

The mean and the maximum peak gust velocity coefficients are derived from the wind tunnel test by the following relation:

$$\hat{C}_V = \overline{C}_V + g.\sigma_V \tag{5.1}$$

where:

 $\hat{C}_{\scriptscriptstyle V}$  is the 3-second gust velocity coefficient.

- $\overline{C}_{V}$  is the mean velocity coefficient.
- g is the gust factor, which is taken to be 3.0 for a 3s gust and 3.4 for a 0.5s gust
- $\sigma_{\scriptscriptstyle V}\,$  is the standard deviation of the velocity measurement.

The mean free-stream wind speed measured in the wind tunnel for this study was approximately 10.8m/s. Note that the measurement location for the mean free-stream wind speed is at a height of 200m at the upwind edge of the proximity model. A sampling time of 12 seconds was used for each wind direction tested, which is equivalent to a minimum sample time of approximately 34 minutes in full-scale for the annual maximum gust wind speeds, suitable for this type of study.

#### 5.2 Calculation of the Full-Scale Results

To determine if the wind conditions at each study point location will satisfy the relevant criteria for pedestrian comfort and safety, the measured velocity coefficients need to be combined with information about the local wind climate. The aim of combining the wind tunnel measurements with wind climate information is to determine the probability of exceedance of a given wind speed at the site. The local wind climate is normally described using a statistical model, which relates wind speed to a probability of exceedance. Details of the wind climate model used in this study are outlined in Section 1.

A feature of this process is to include the impact of wind directionality, which includes any local variations in wind speed or frequency with wind direction. This is important as the wind directions which produce the highest wind speed events for a region may not coincided with the most wind exposed direction at the site.

The methodology adopted for the derivation of the full-scale results for the annual maximum gust and the weekly maximum GEM wind speeds are outlined in the following sub-sections.

#### 5.2.1 Annual Maximum Gust Wind Speeds

The full-scale annual maximum gust wind speed at each study point location is derived from the measured velocity coefficient using the following relationship:

$$V_{study} = V_{ref,RH} \left( \frac{k_{200m,tr,T=3600s}}{k_{RH,tr,T=3600s}} \right) C_V$$
(5.2)

 $V_{\rm study}$  is the full-scale wind velocity at the study point location, in m/s.

- $V_{ref,RH}$  is the full-scale reference wind speed at the upwind edge of the proximity model at the study reference height. This value is determined by combining the directional wind speed data for the region (detailed in Section 1) and the upwind terrain and height multipliers for the site (detailed in Section 3).
- $k_{200m,tr,T=3600s}$  is the hourly mean terrain and height multiplier at 200m for the standard terrain category setup used in the wind tunnel tests.
- $k_{RH,tr,T=3600s}$  is the hourly mean terrain and height multiplier at the study reference height (see Table 3).
  - $C_V$  is the velocity coefficient measurement obtained from the hot-wire anemometer, which is derived from the following relationship:

$$C_V = \frac{C_{V,study}}{C_{V,200m}}$$
(5.3)

- $C_{V, study} \quad \mbox{is the velocity coefficient measurement obtained from the hotwire anemometer at the study point location.}$
- $C_{\!_{V,200m}} \qquad \hbox{is the measurement obtained from the hot-wire anemometer} \\ {\rm at the free-stream reference location at 200m height upwind} \\ {\rm of the model in the wind tunnel.} \\ \end{tabular}$

The value of  $V_{ref,RH}$  varies with each prevailing wind direction. Wind directions where there is a high probability that a strong wind will occur will have a higher directional wind speed than other directions. To determine the directional wind speeds, a probability level must be assigned for each wind direction. These probability levels are set following the approach used in AS/NZS1170.2:2011, which assumes that the major contributions to the combined probability of exceedance of a typical load effect comes from only two 45deg sectors.

#### 5.2.2 Weekly Maximum Gust-Equivalent Mean Wind Speeds

The contribution to the probability of exceedance of a specified wind speed (i.e.: the desired wind speed for pedestrian comfort, as per the criteria) is calculated for each wind direction. These contributions are then combined over all wind directions to calculate the total probability of exceedance of the specified wind speed. To calculate the probability of exceedance for a specified wind speed a statistical wind climate model was used to describe the relationship between directional wind speeds and the probability of exceedance. A detailed description of the methodology is given by T.V. Lawson (1980).

The criteria of A.G. Davenport (1972), which is used in this study, is referenced to a probability of exceedance of 5.5% of a specified wind speed and is representative of approximately a weekly recurrence interval.

#### 5.3 Layout of Study Points

For this study, a total of 42 study point locations has been selected for analysis in the wind tunnel. The locations of the various study points tested for this study are presented in Figures 5a to 5d in the form of a marked-up plan drawings, along with the wind criteria each point is required to meet. It should be noted that only the most critical outdoor locations of the development have been selected for analysis.

#### **Target Criteria**

A.G. Davenport (1972) criterion of 5.5m/s (weekly GEM's) for short exposure activities. W.H. Melbourne (1978) criterion of 23m/s (annual gusts) for safety.



A.G. Davenport (1972) criterion of 7.5m/s (weekly GEM's) for pedestrian activities. W.H. Melbourne (1978) criterion of 23m/s (annual gusts) for safety.

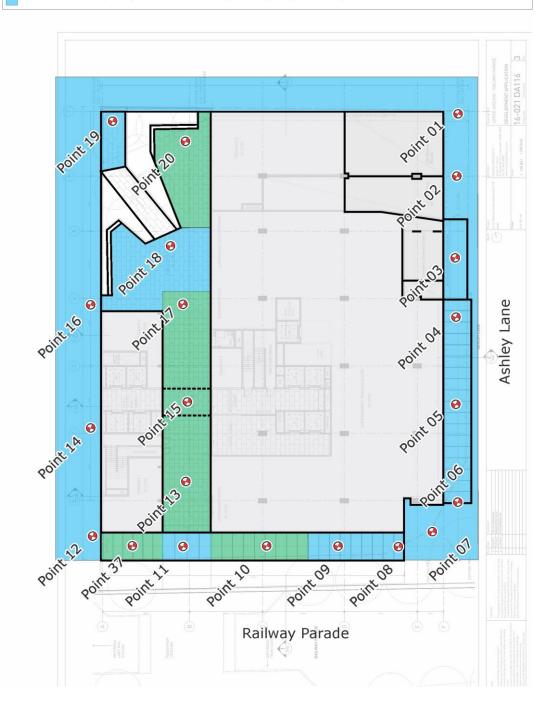


Figure 5a: Study Point Locations and Wind Speed Criteria – Ground Level Areas along Railway Parade and Ashley Lane



Figure 5b: Study Point Locations and Wind Speed Criteria – Level 3 (Hotel Lobby)

#### Target Criteria

A.G. Davenport (1972) criterion of 5.5m/s (weekly GEM's) for pedestrian activities. W.H. Melbourne (1978) criterion of 23m/s (annual gusts) for safety.

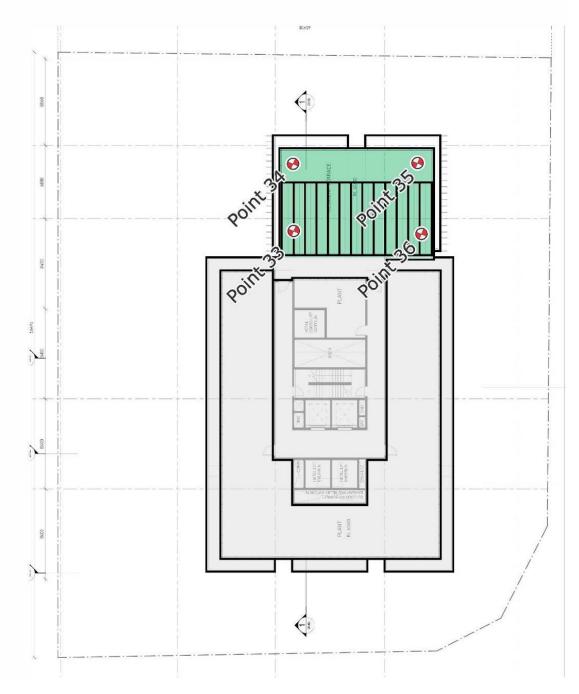


Figure 5c: Study Point Locations and Wind Speed Criteria – Level 8 (Plant Room)

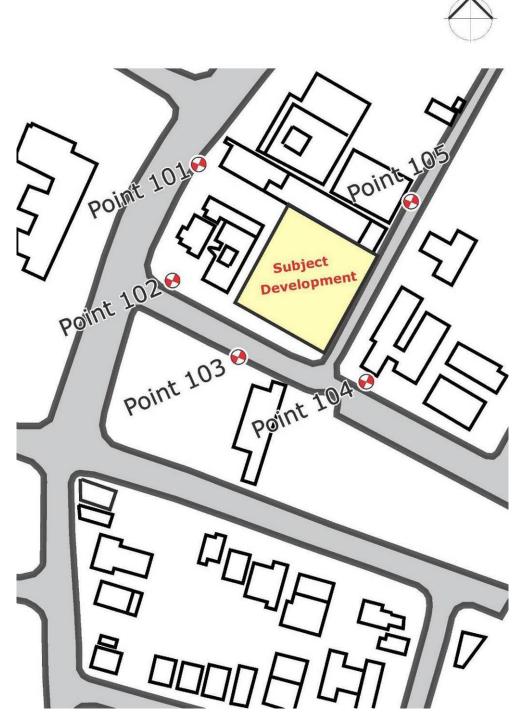


Figure 5d: Study Point Locations and Wind Speed Criteria – Surrounding Location

The model of the development was initially tested in the wind tunnel without the effects of any form of wind ameliorating devices such as screens, balustrades, etc., which are not already shown in the architectural drawings. The effect of vegetation was also excluded from the initial testing. Wind rose plots of the various study points from the initial wind tunnel study (without any treatments) are illustrated in Figures 6a to 6d.



Figure 6a: Wind Directionality Plots for Proposed Scenario – Ground Level Areas along Railway Parade and Ashley Lane

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Figure 6b: Wind Directionality Plots for Proposed Scenario – Level 3 (Hotel Lobby)

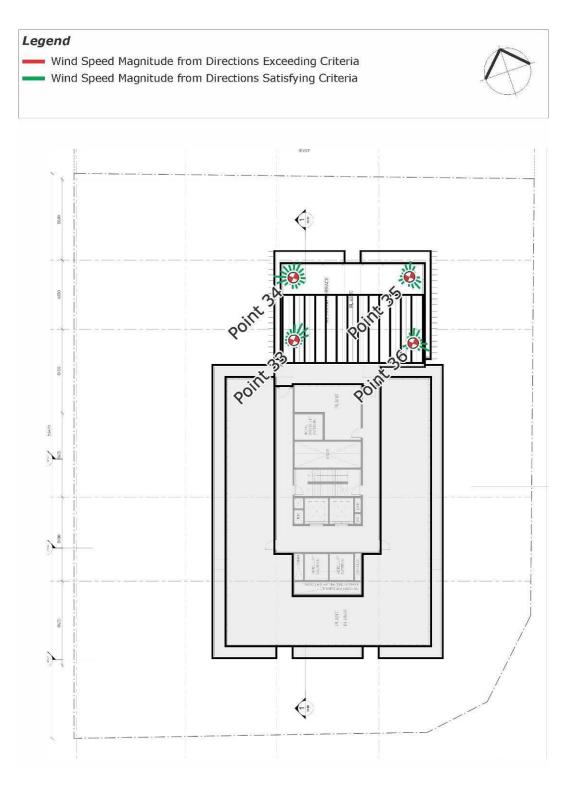


Figure 6c: Wind Directionality Plots for Proposed Scenario – Level 8 (Plant Room)

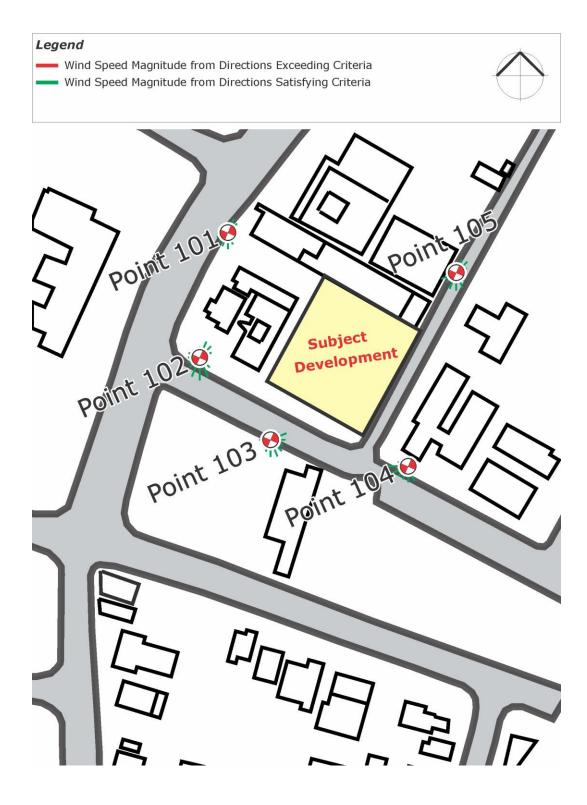


Figure 6d: Wind Directionality Plots for Existing Scenario – Surrounding Areas

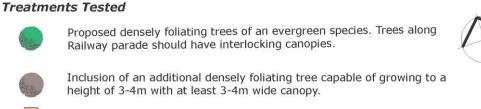
The results of the study indicate that treatments are required for certain locations to achieve the desired wind speed criteria for pedestrian comfort and safety to the various public and communal areas. The following treatments, which are also detailed in the marked-up plans presented in Figures 7a and 7b, have been tested as part of the wind tunnel study to verify their effectiveness:

#### **Ground Level Areas**

- Inclusion of the proposed densely foliating trees with interlocking canopies along the southern perimeter (Railway Parade).
- Inclusion of an additional densely foliating tree capable of growing to a height of 3-4m with at least 3-4m wide canopy at the south-western corner of the development.
- Extension of the proposed eastern and southern awnings to connect at the southeastern corner.
- Glaze in the opening at the southern end of the atrium, for the section above the awning along Railway Parade.

#### Level 3 (Hotel Lobby)

- Inclusion of proposed landscaping for the Level 3 Terrace.
- Extension of the proposed densely foliating evergreen hedge at the north-eastern corner of the terrace space. The hedge needs to be capable of growing to a height of 1.5m.
- Make the proposed awning on Level 3 Terrace to be impermeable.



Extension of proposed eastern and southern awnings at the south-eastern corner.

Glaze in the opening at the southern end of the atrium, for the section above the awning along Railway Parade.

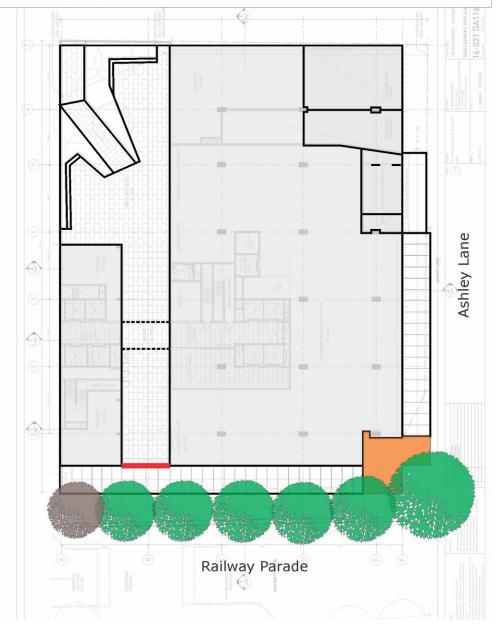


Figure 7a: Treatments Tested in the Wind Tunnel – Ground Level Areas along Railway Parade and Ashley Lane



Figure 7b: Treatments Tested in the Wind Tunnel – Level 3 (Hotel Lobby)

The results for all study points locations including the tested treatments are presented in the form of directional plots in Appendix A, and are summarised in Table 9. The wind speed criteria that the wind conditions should achieve are also listed in Table 9 for each study point location, as well as in Figures 5a and 5d.

A comparative analysis of the wind directional plots for the various study points indicates that a revised treatment strategy is necessary to achieve the desired wind speed criteria for pedestrian comfort and safety at the south-western corner of the subject development. For the proposed development with treatments, it has been observed that southerly winds directly impact the Ground Level areas and sidestream along the southern boundary of the development, gaining momentum. These winds can then further accelerate around the south-western corner leading to undesirable wind speeds at the location. To achieve the desired wind speed criteria for pedestrian comfort, the following in-principle treatments, in addition to the tested treatments, are recommended for the Ground Level areas:

- Inclusion of 1.2m high portable operator-controlled screens at the south-western corner of the subject development if this area is to be used for seating such as for outdoor café seating. Wind conditions in this section of the building frontage currently satisfy the comfortable walking criterion without the portable screens. The area is marked out in Figure 8.
- Extension of proposed southern awning towards the south-eastern corner of the subject development. The proposed extension to the southern awning will be sufficient to improve the wind conditions at the south-eastern corner. The extended awning is illustrated in Figure 8.

With the inclusion of these treatments, it is expected that wind conditions for all outdoor trafficable areas around the subject will be suitable for their uses.

Study		Criterion /s)	Equivalent or Better than	Treatment Necessary	Description of Tested	Description of Additional
Point	Weekly GEM	Annual Peak	Existing Site Conditions?	to Pass?	Treatment/Notes	In-Principle Treatments
Point 01	7.5	23.0	YES	NO	-	-
Point 02	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 03	7.5	23.0	YES	NO	-	-
Point 04	7.5	23.0	YES	NO	-	-
Point 05	7.5	23.0	YES	NO	-	-
Point 06	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 07	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 08	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 09	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 10	5.5	23.0	NO	YES	Refer to Figure 7a	-
Point 11	7.5	23.0	NO	YES	Refer to Figure 7a	-
Point 12	7.5	23.0	NO	YES	Refer to Figure 7a	Refer to Figure 8
Point 13	5.5	23.0	-	NO	-	-
Point 14	7.5	23.0	-	YES	Refer to Figure 7a	-

#### **Table 9: Treatment Results Summary**

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Study Point	Desired Criterion (m/s)		Equivalent or Better than	Treatment Necessary	Description of Tested	Description of Additional
	Weekly GEM	Annual Peak	Existing Site Conditions?	to Pass?	Treatment/Notes	In-Principle Treatments
Point 15	5.5	23.0	-	YES	Refer to Figure 7a	-
Point 16	7.5	23.0	-	NO	-	-
Point 17	5.5	23.0	-	YES	Refer to Figure 7a	-
Point 18	7.5	23.0	-	NO	-	-
Point 19	7.5	23.0	-	NO	-	-
Point 20	5.5	23.0	-	NO	-	-
Point 25	5.5	23.0	-	YES	Refer to Figure 7b	-
Point 26	5.5	23.0	-	YES	Refer to Figure 7b	-
Point 27	5.5	23.0	-	YES	Refer to Figure 7b	-
Point 28	5.5	23.0	-	YES	Refer to Figure 7b	-
Point 29	5.5	23.0	-	NO	-	-
Point 33	5.5	23.0	-	NO	-	-
Point 34	5.5	23.0	-	NO	-	-
Point 35	5.5	23.0	-	NO	-	-
Point 36	5.5	23.0	-	NO	-	-
Point 101	7.5	23.0	YES	NO	-	-
Point 102	7.5	23.0	NO	NO	Existing vegetation	-
Point 103	7.5	23.0	NO	NO	-	-
Point 104	7.5	23.0	YES	NO	-	-
Point 105	7.5	23.0	NO	NO	-	-
Point 37	5.5	23.0	-	YES	Refer to Figure 7a	Refer to Figure 8

## **Revised Treatment Strategy**



Retention of proposed densely foliating trees of an evergreen species. Trees along Railway parade should have interlocking canopies.



Inclusion of an additional densely foliating tree capable of growing to a height of 3-4m with at least 3-4m wide canopy.



Inclusion of 1.2m high operator-controlled portable screens if used as an outdoor seating area.

Extension of proposed southern awning at the south-eastern corner.

Glaze in the opening at the southern end of the atrium, for the section above the awning along Railway Parade.

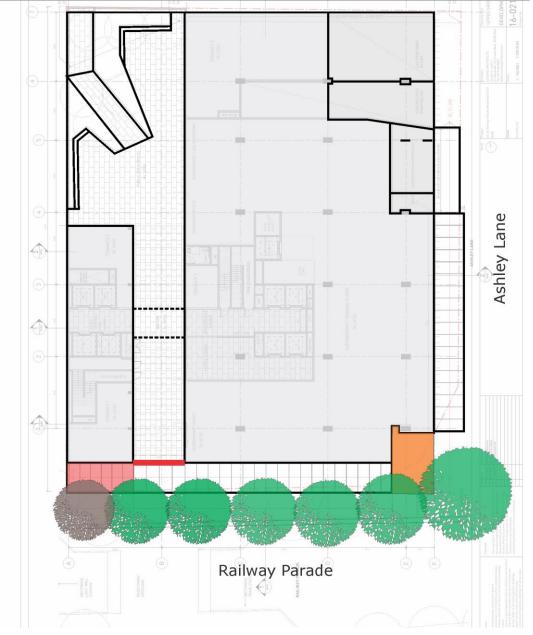


Figure 8: Revised In-Principle Treatment Strategy – Ground Level Areas along Railway Parade and Ashley Lane

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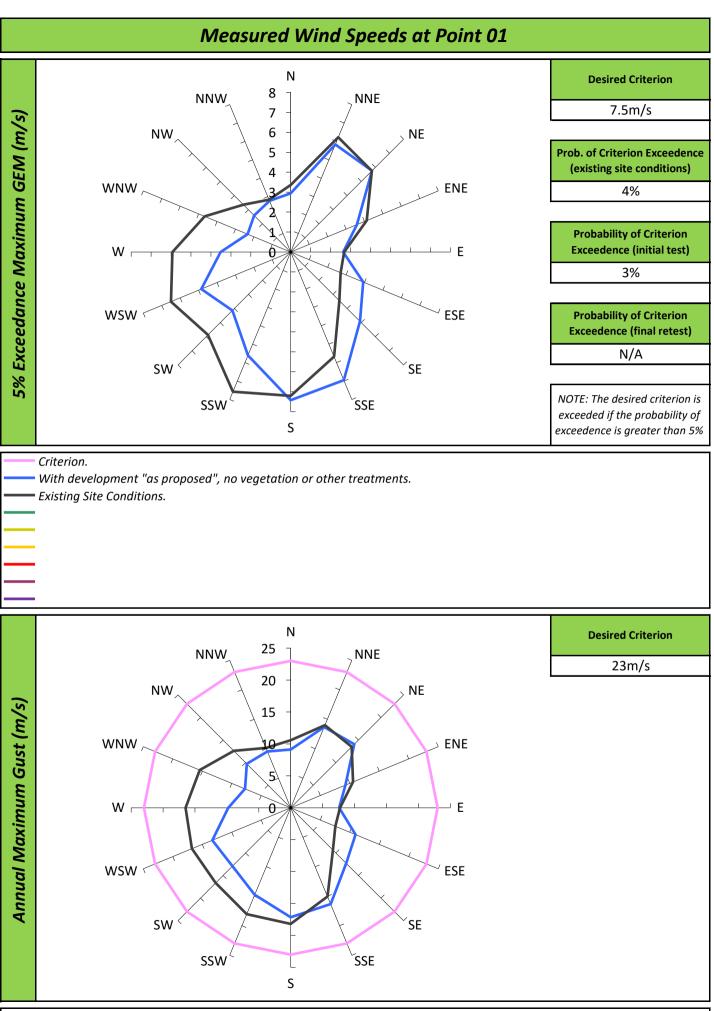
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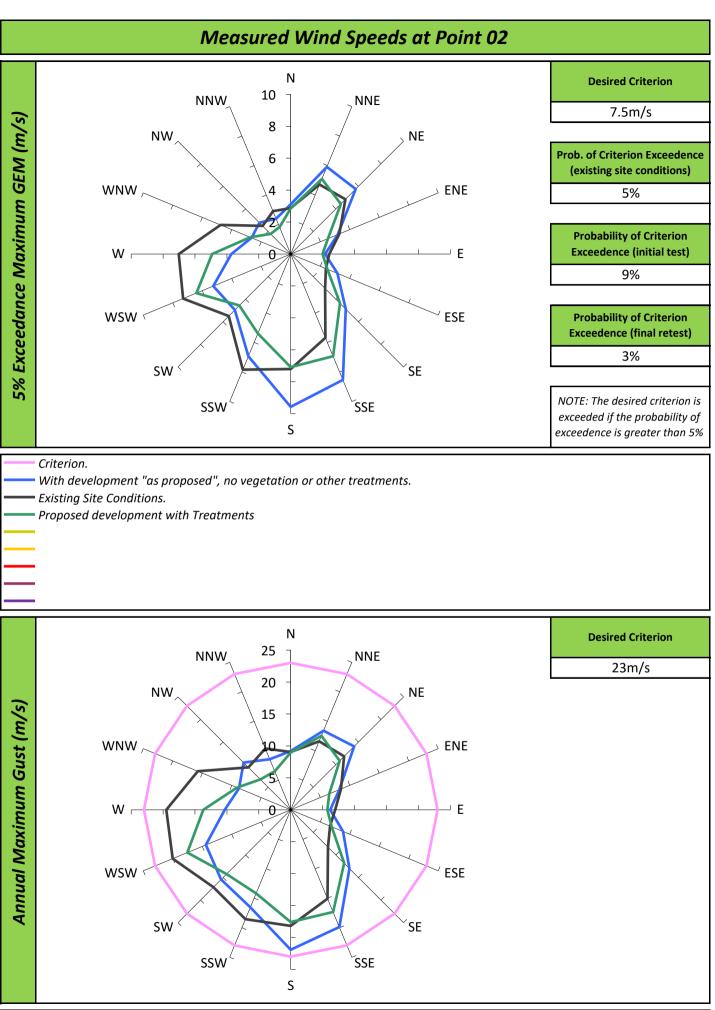
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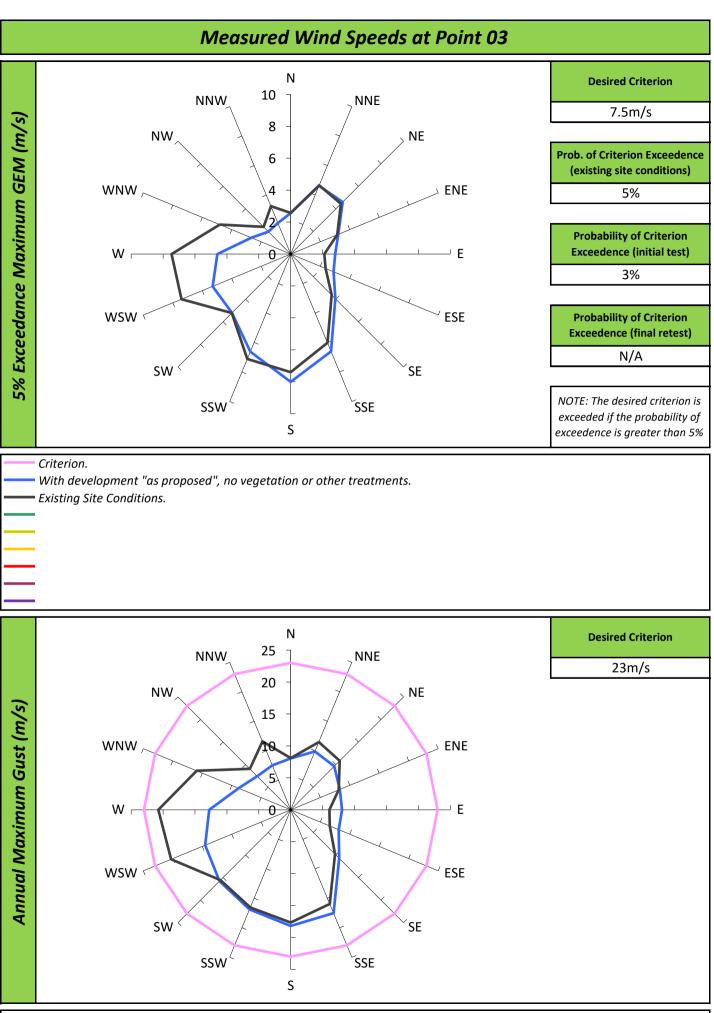
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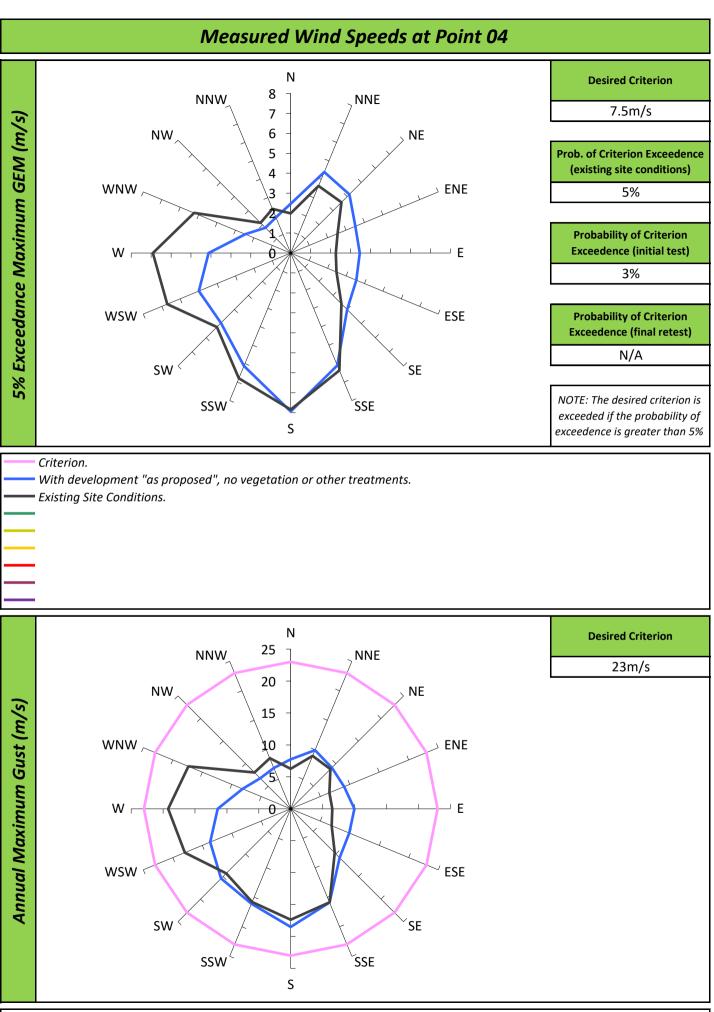
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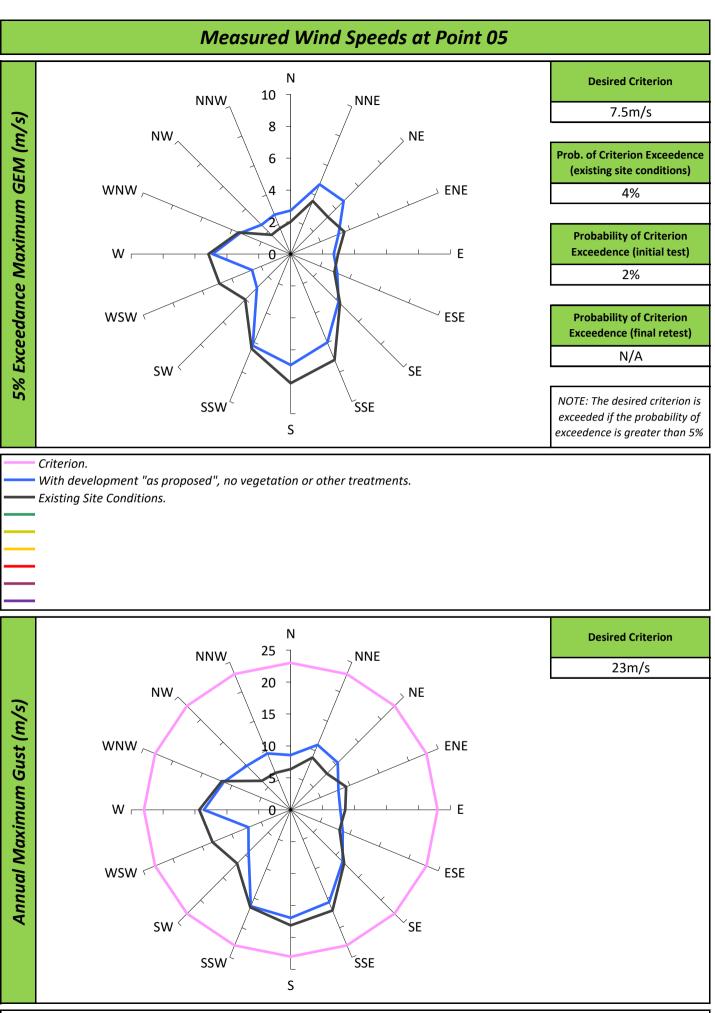
## **APPENDIX A - DIRECTIONAL PLOTS OF THE WIND TUNNEL RESULTS**

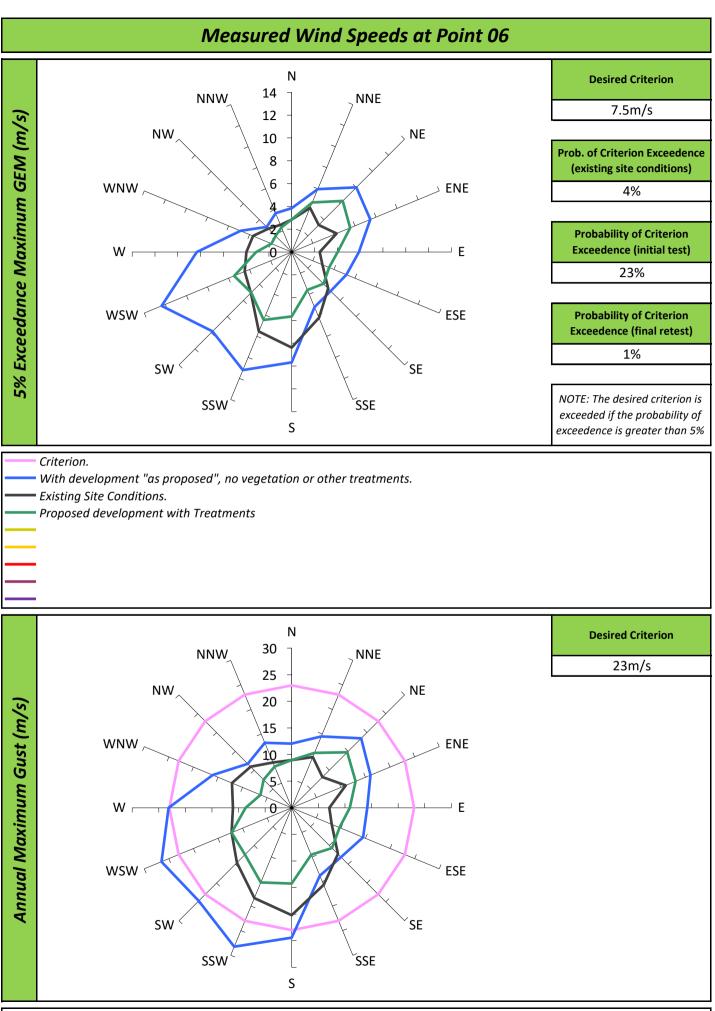


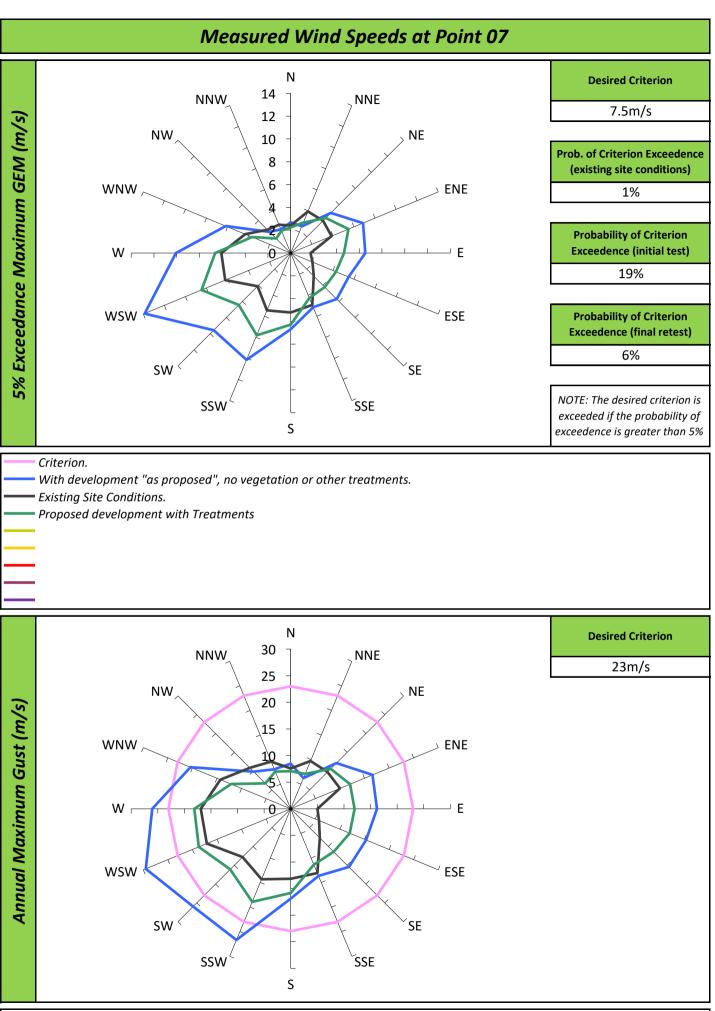


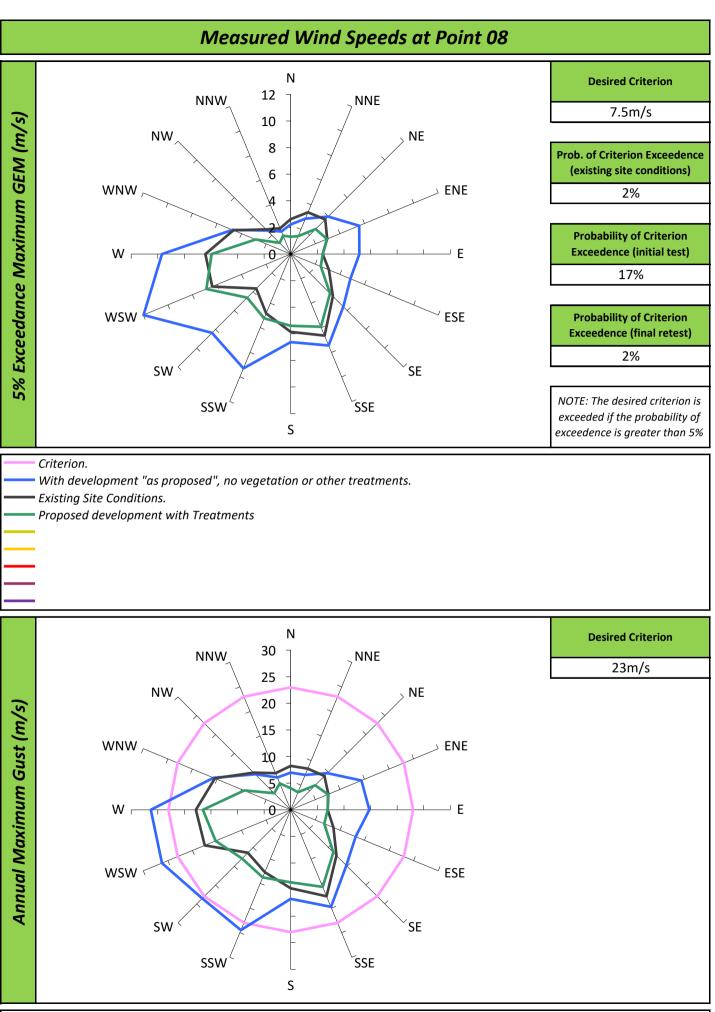


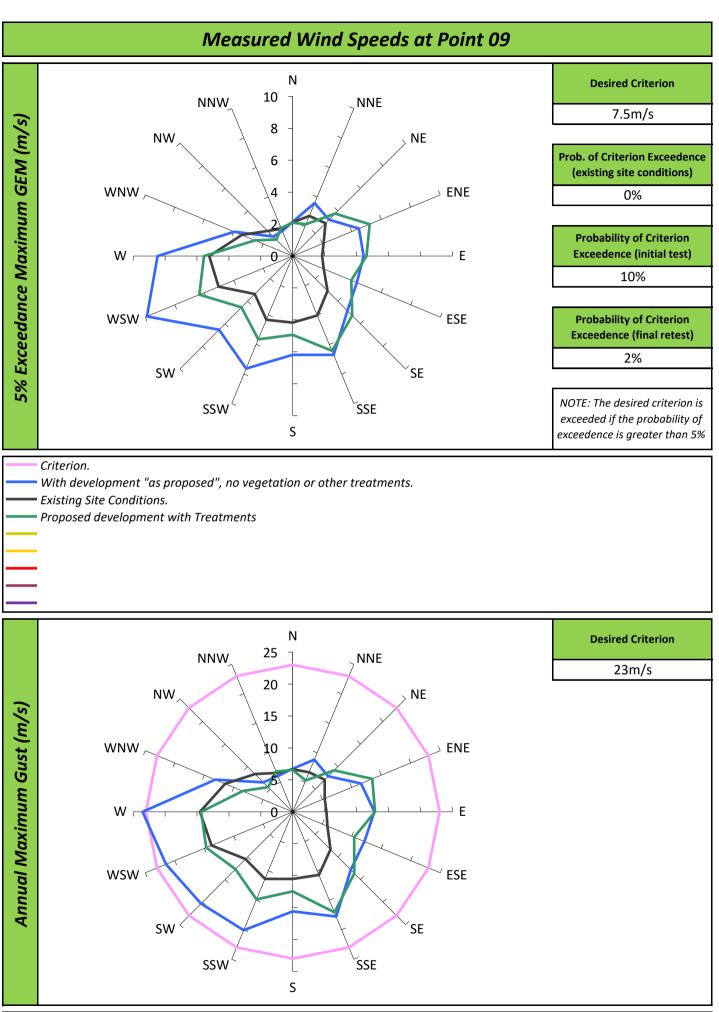


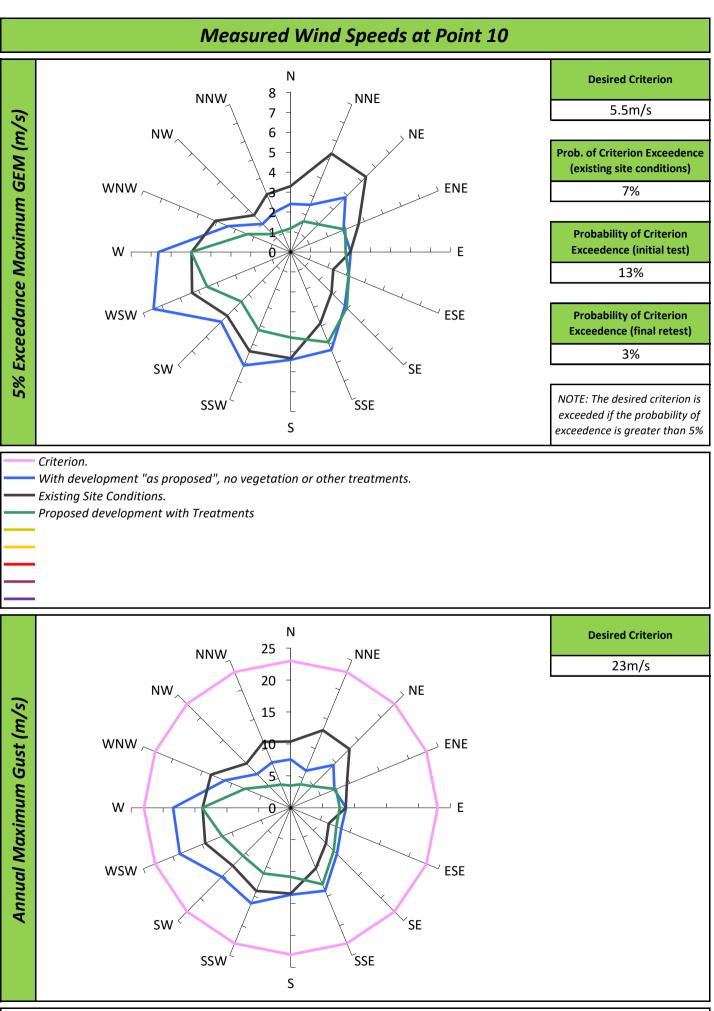


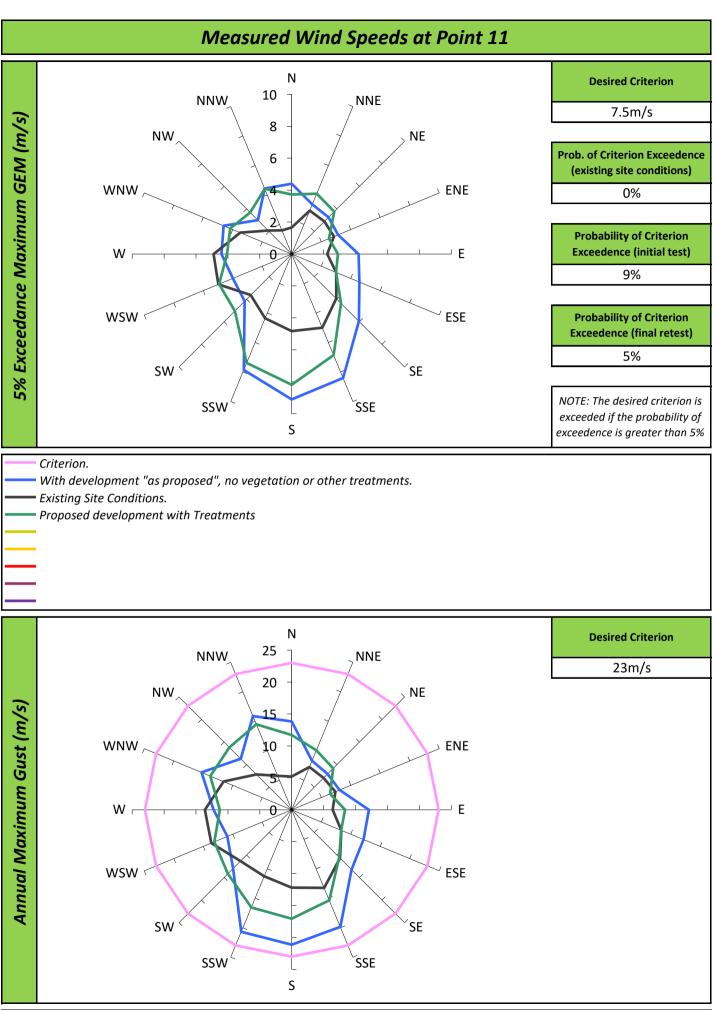


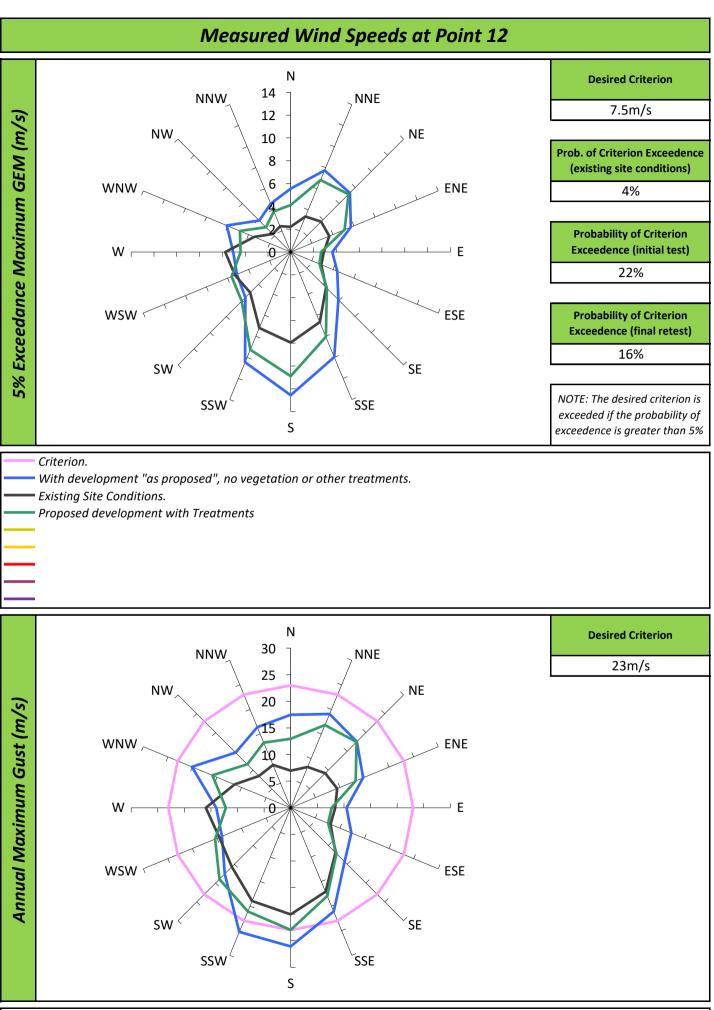


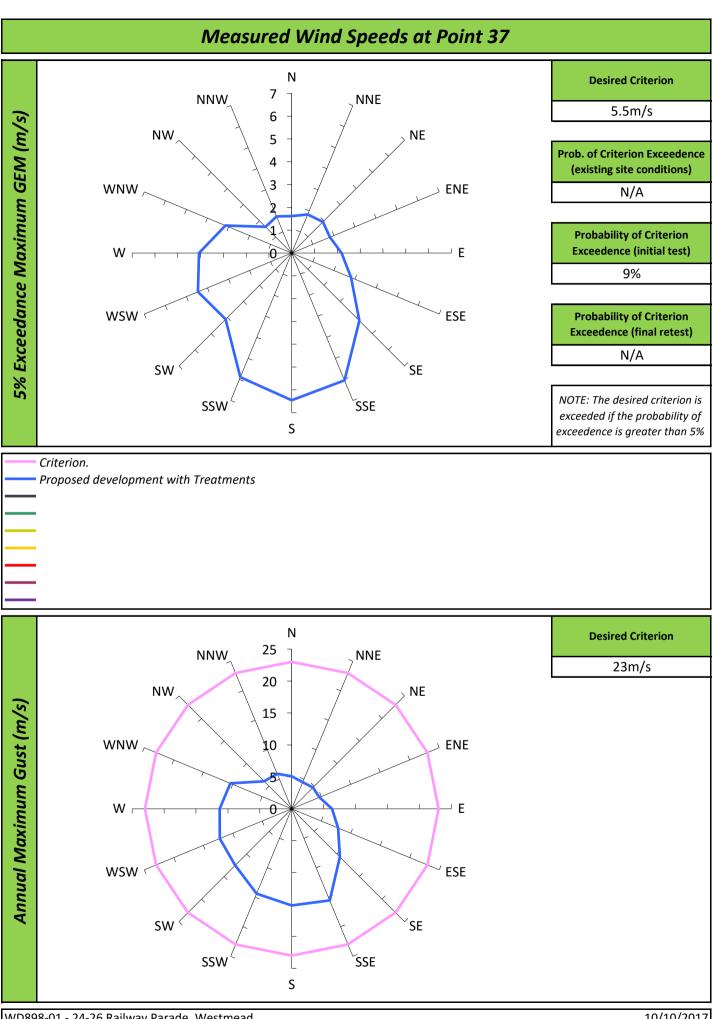


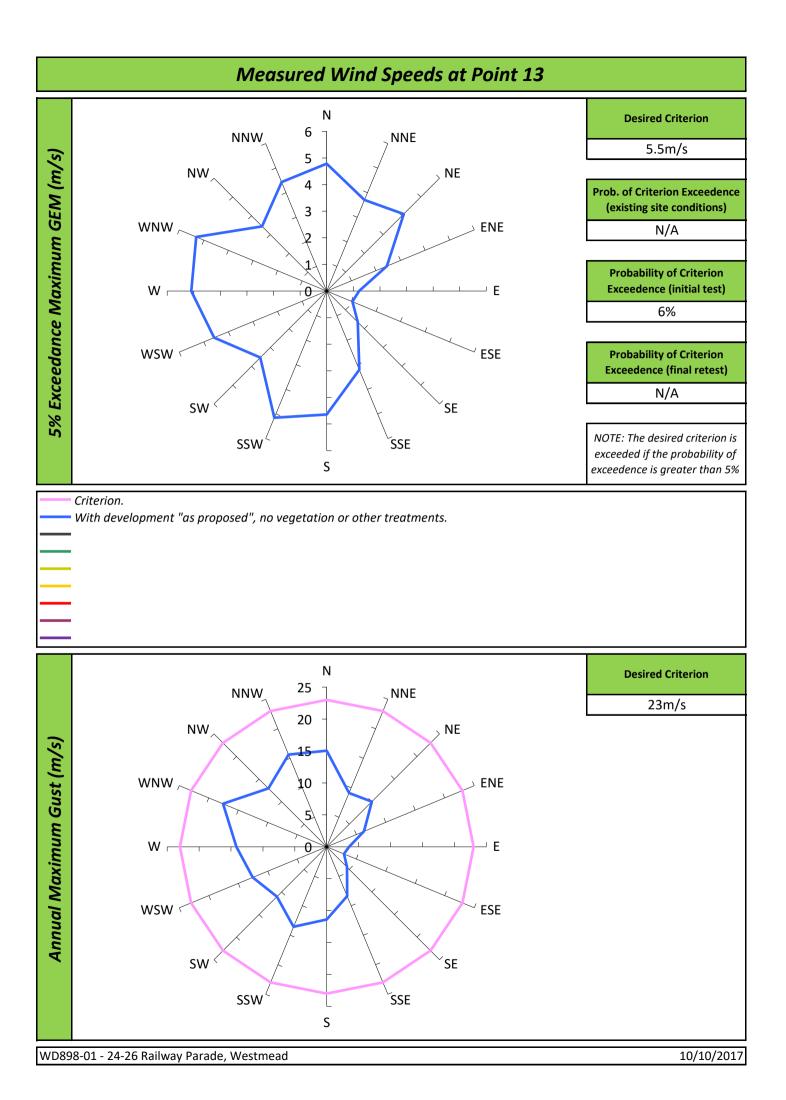


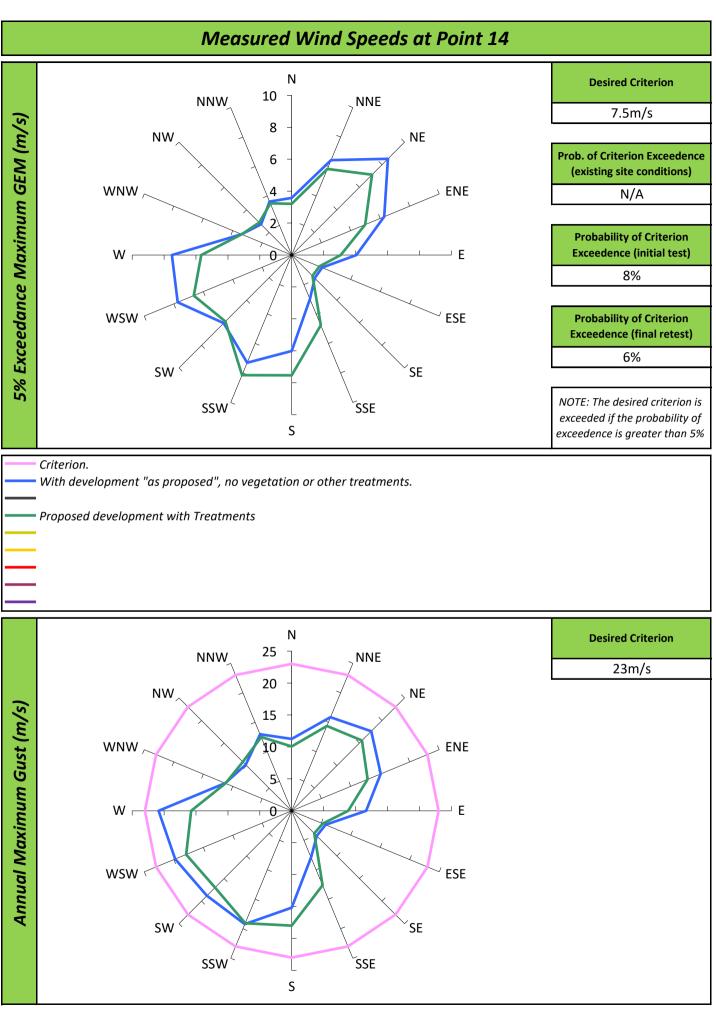


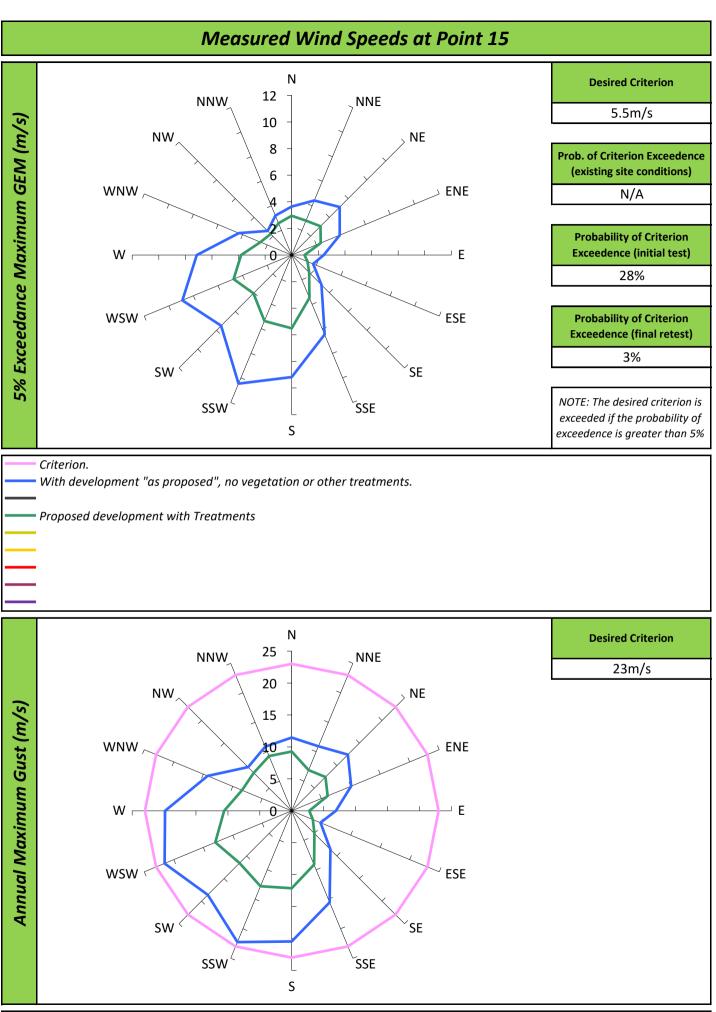


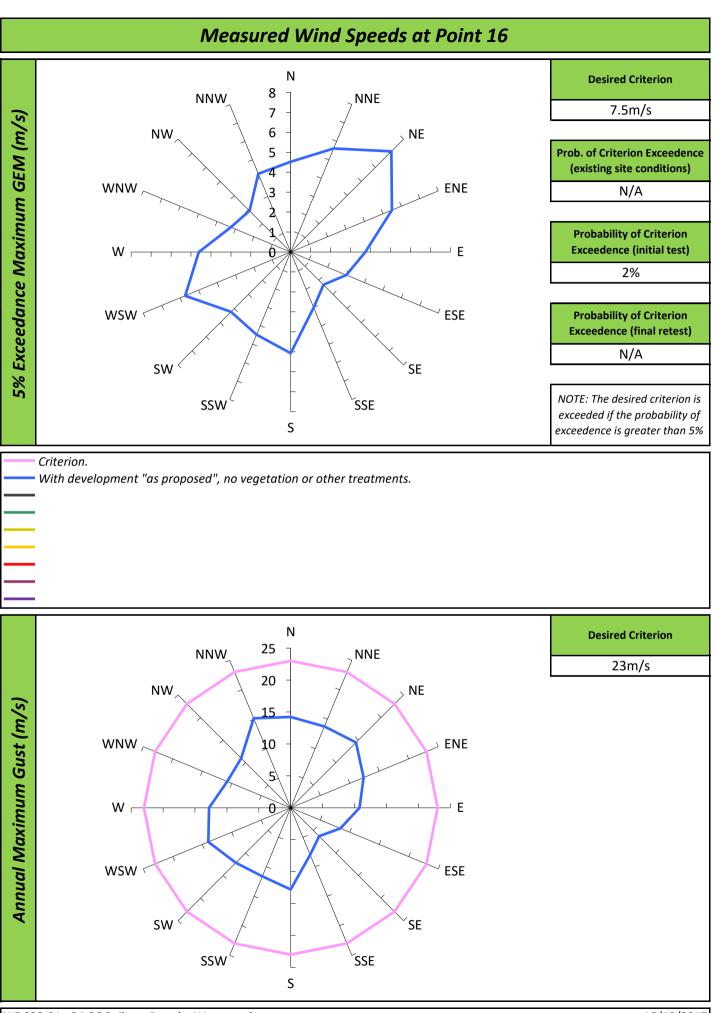


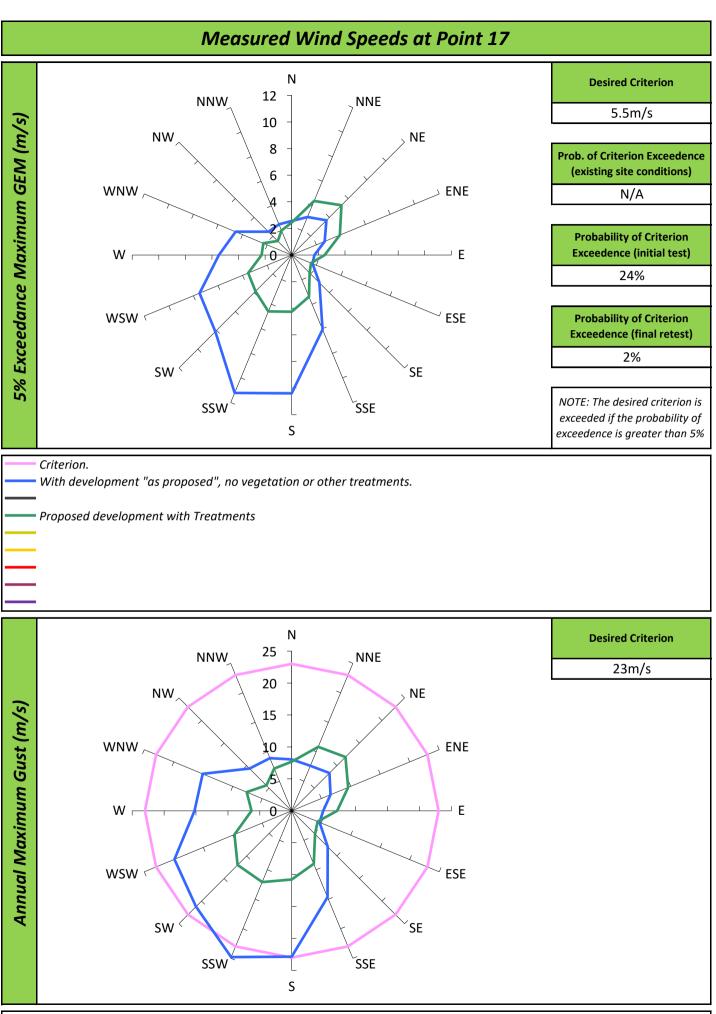


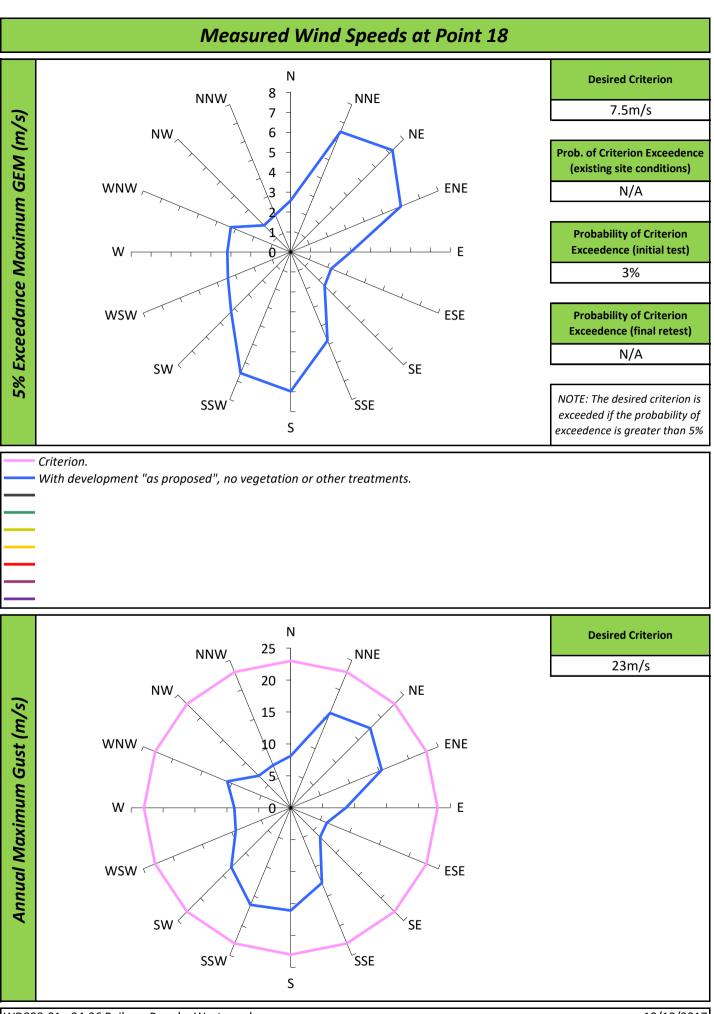


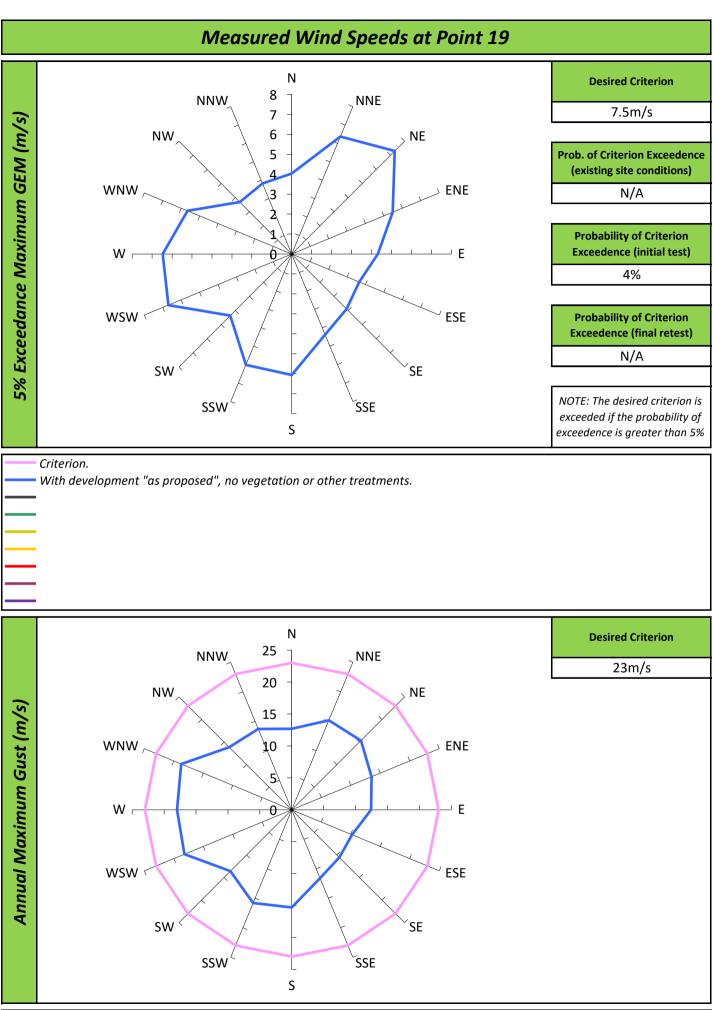


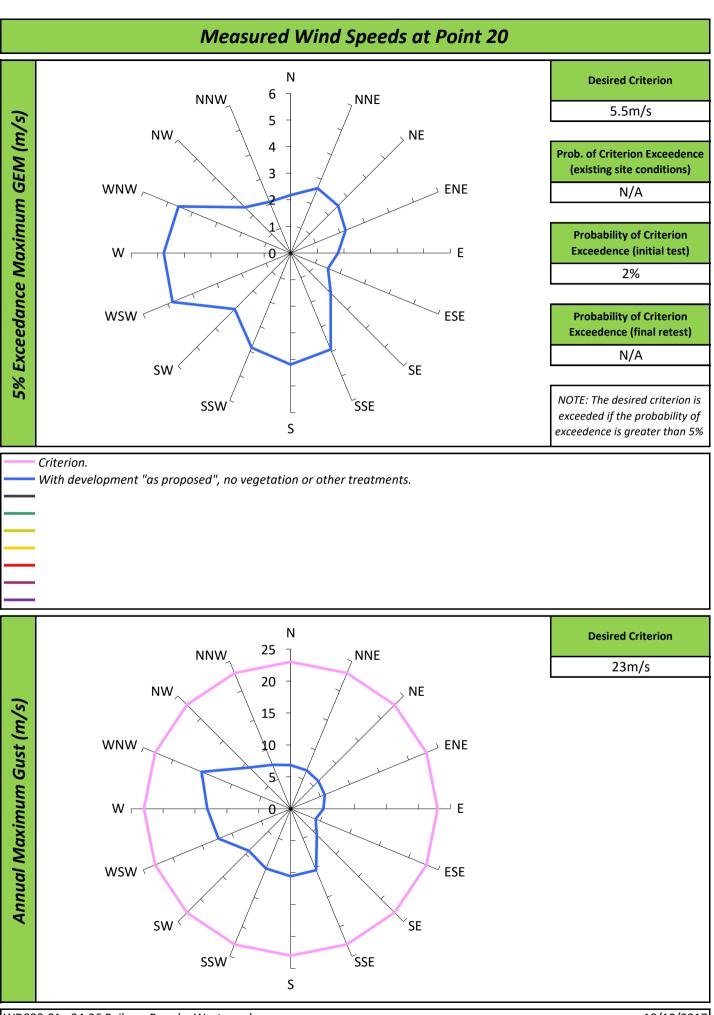


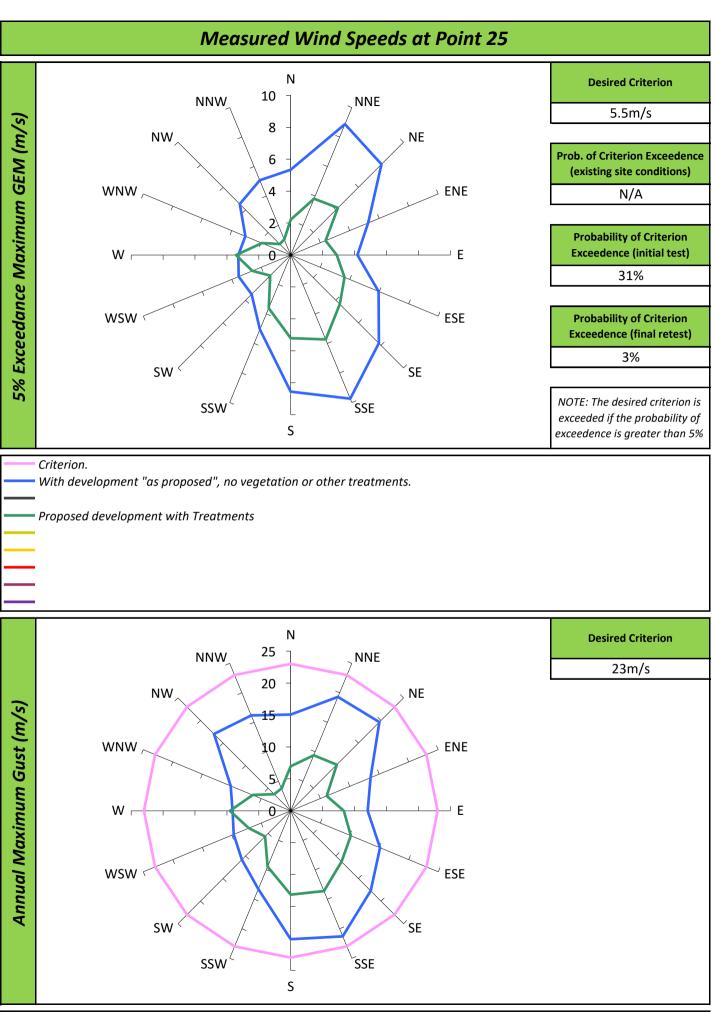


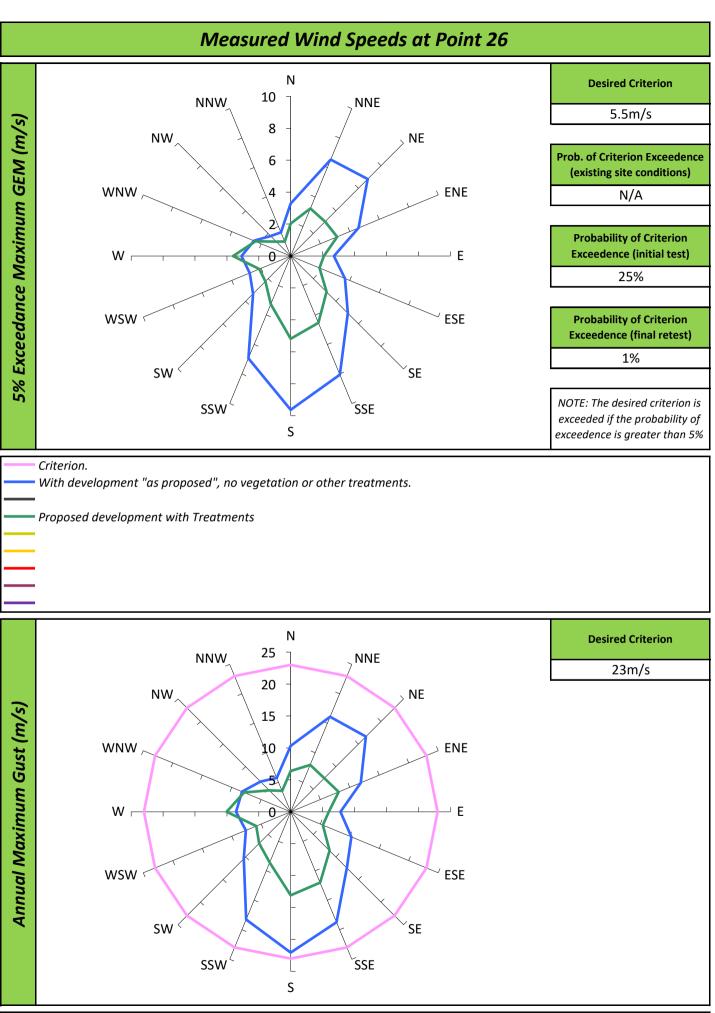


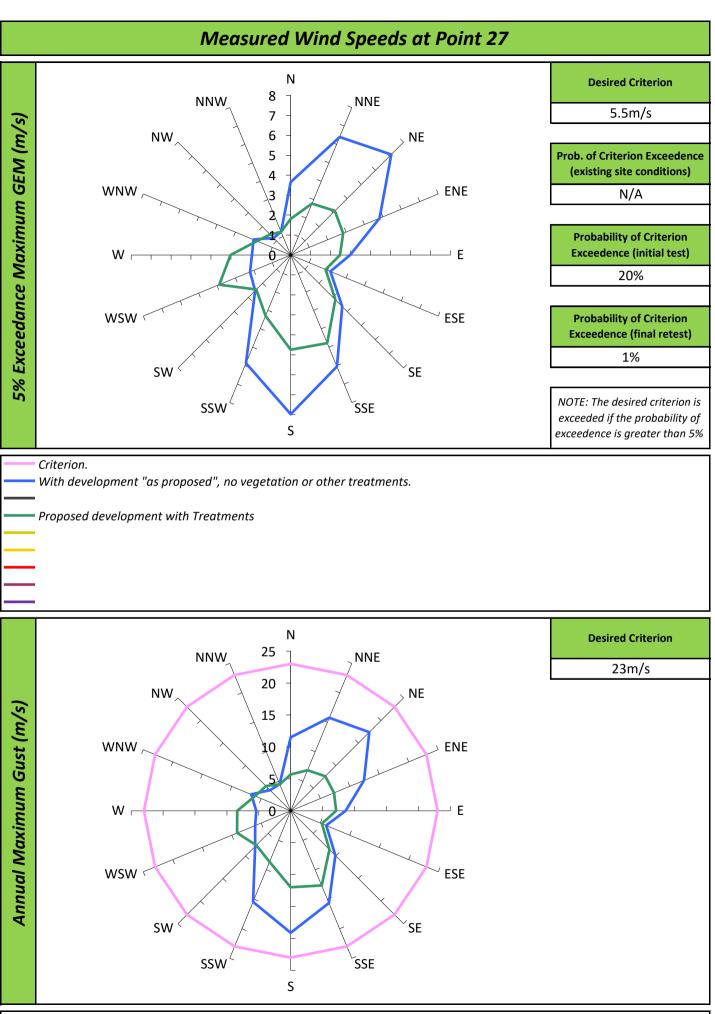


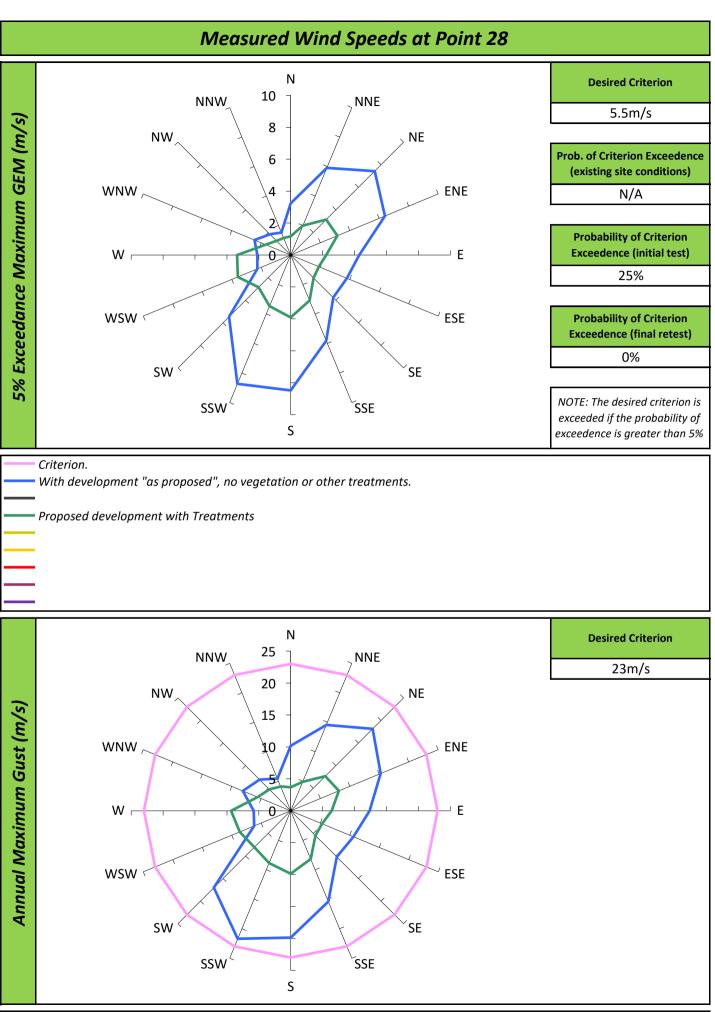


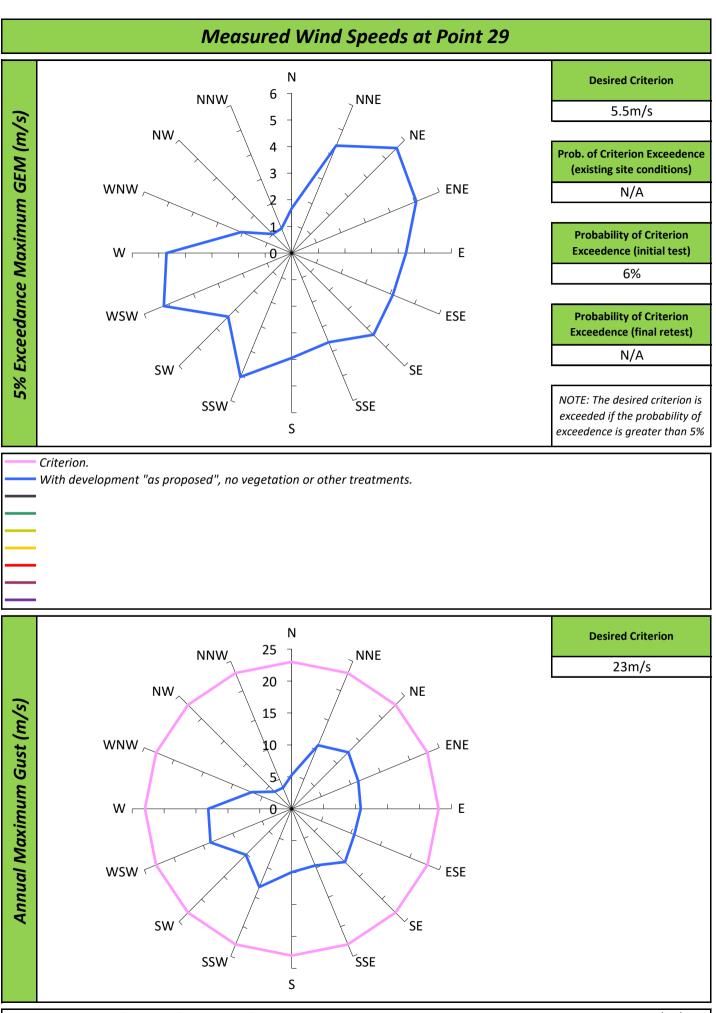


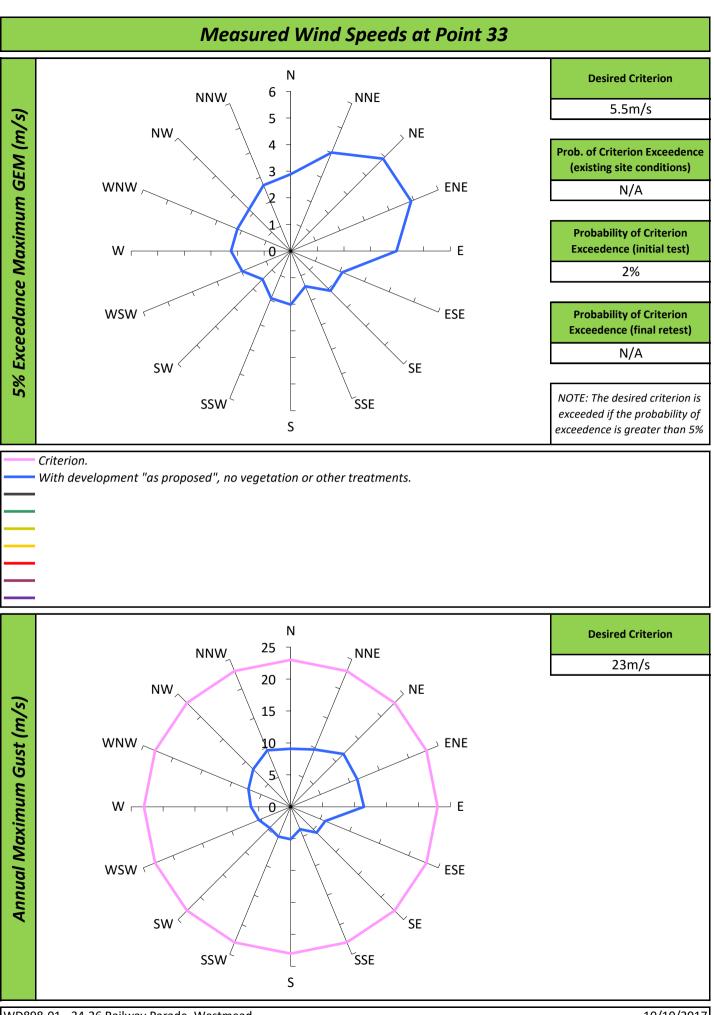


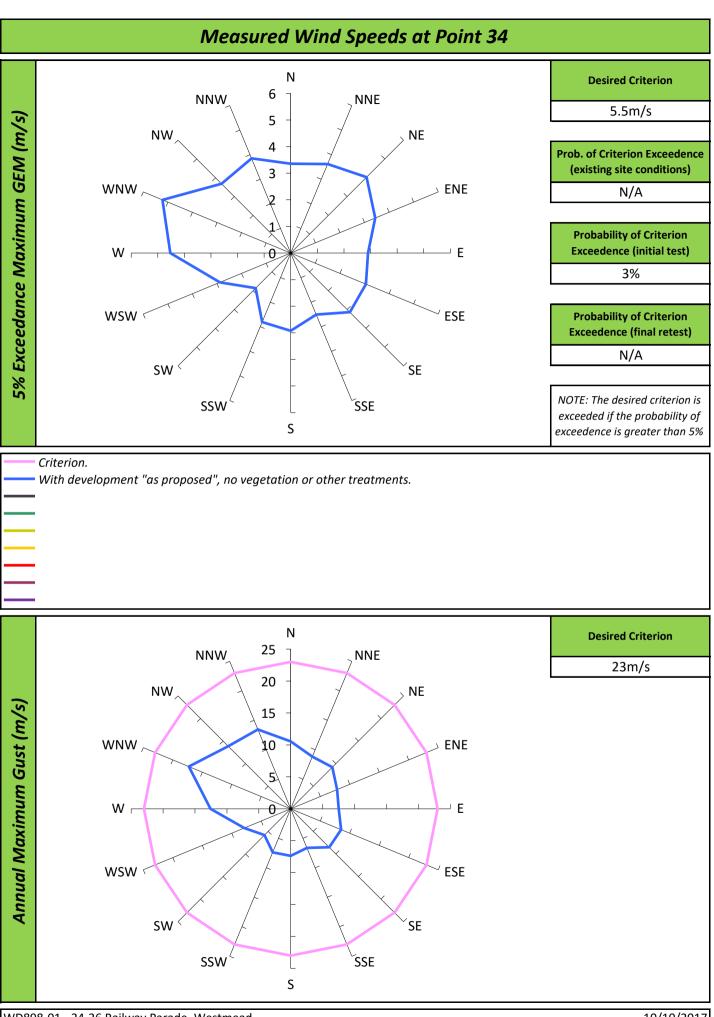


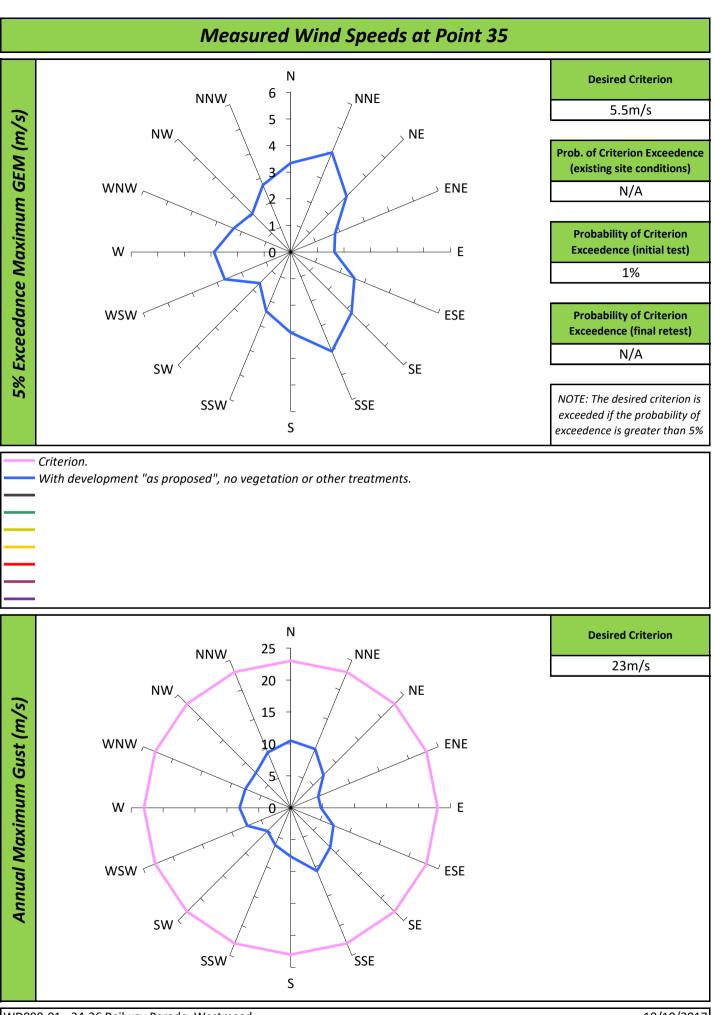


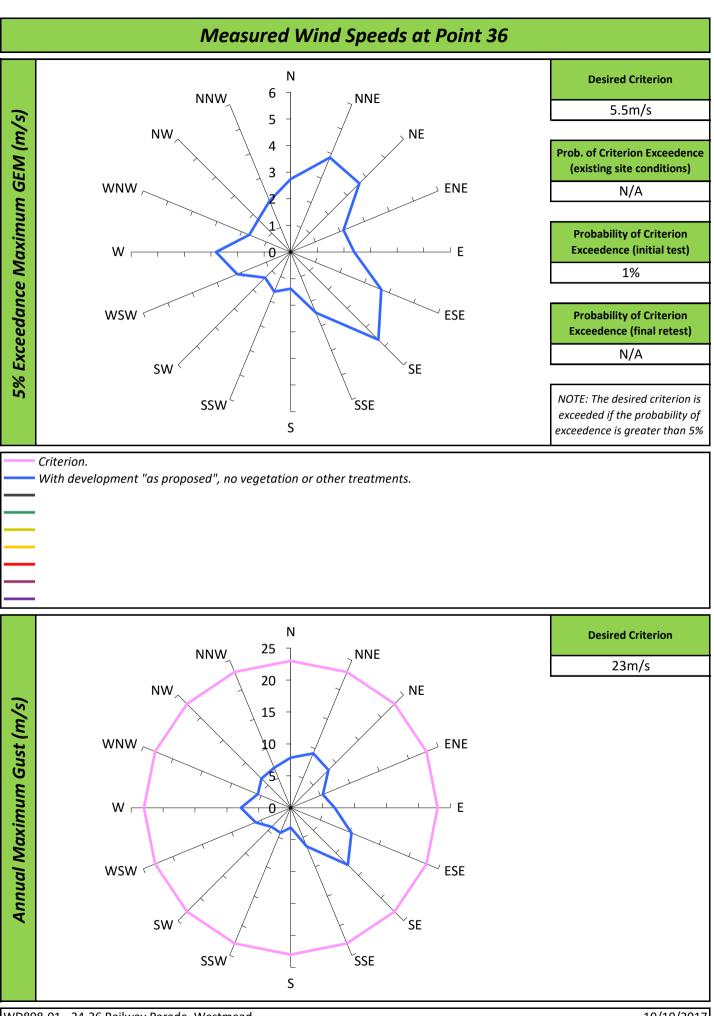


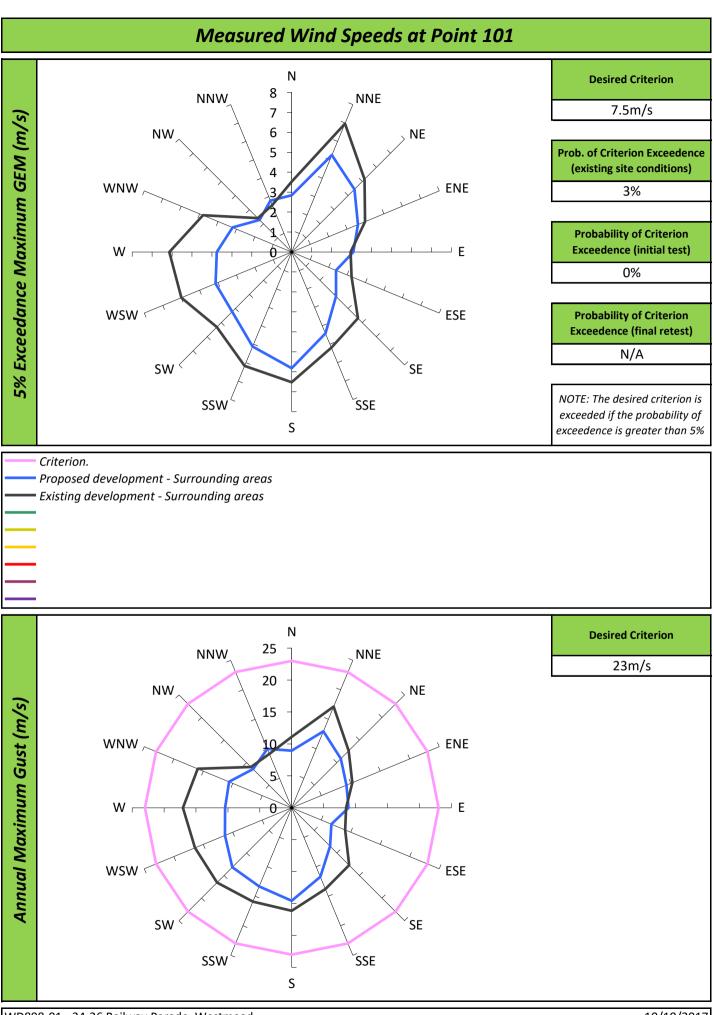


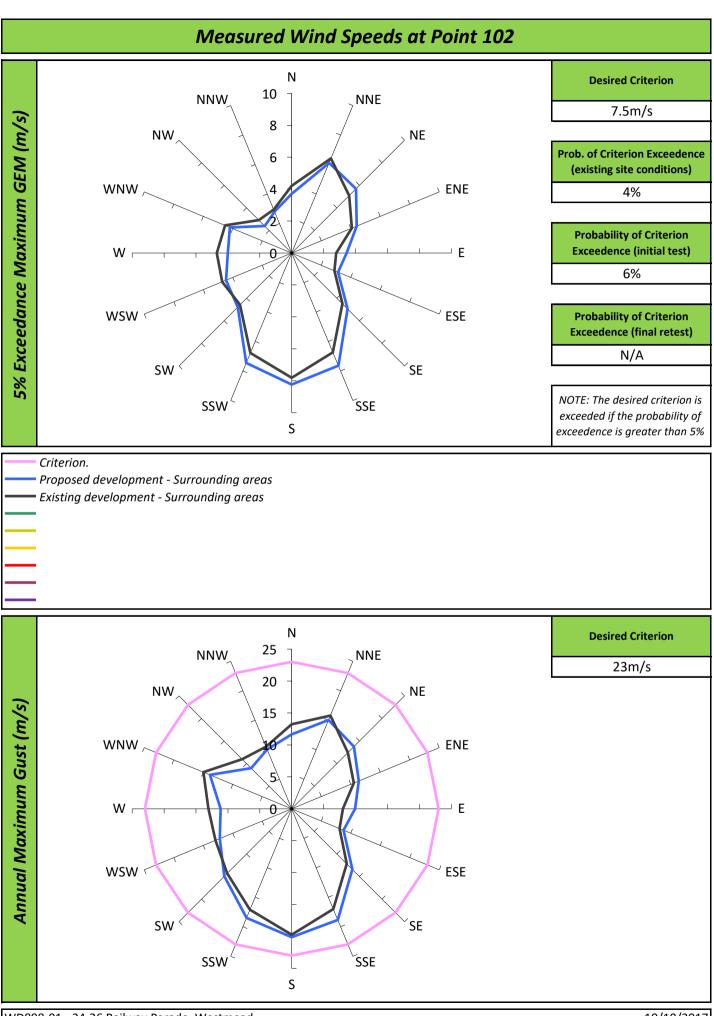


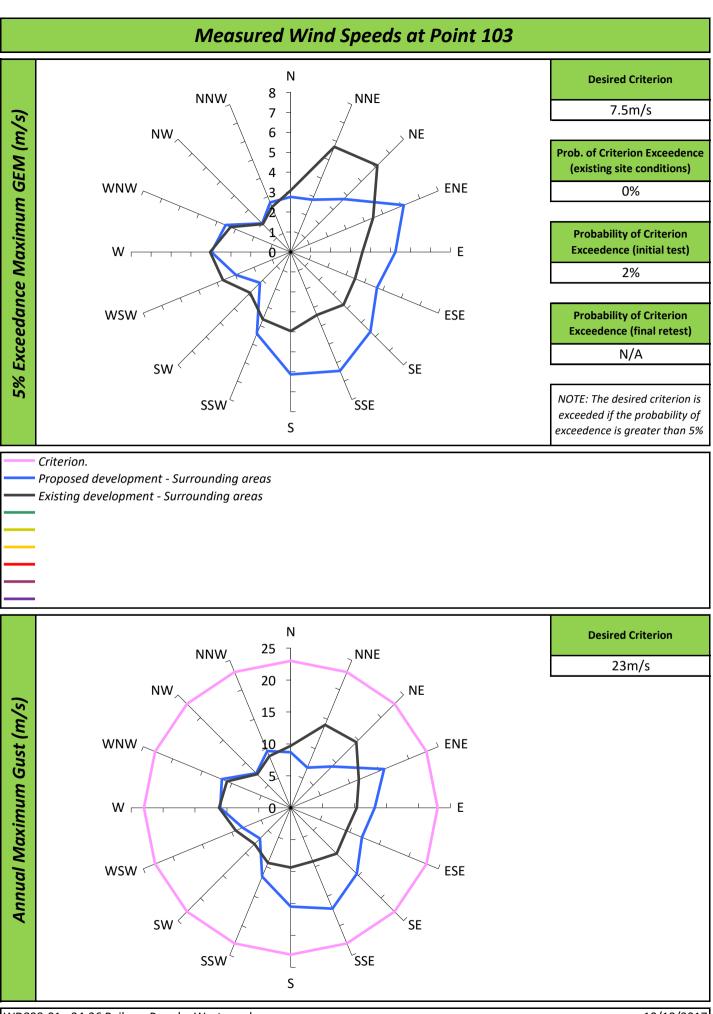


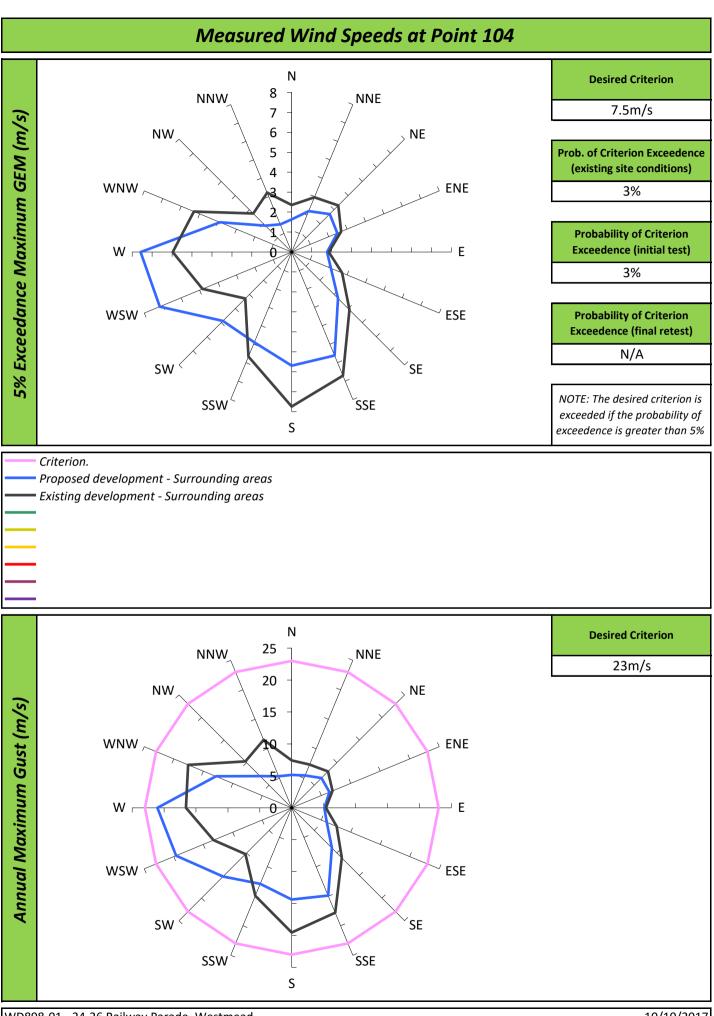


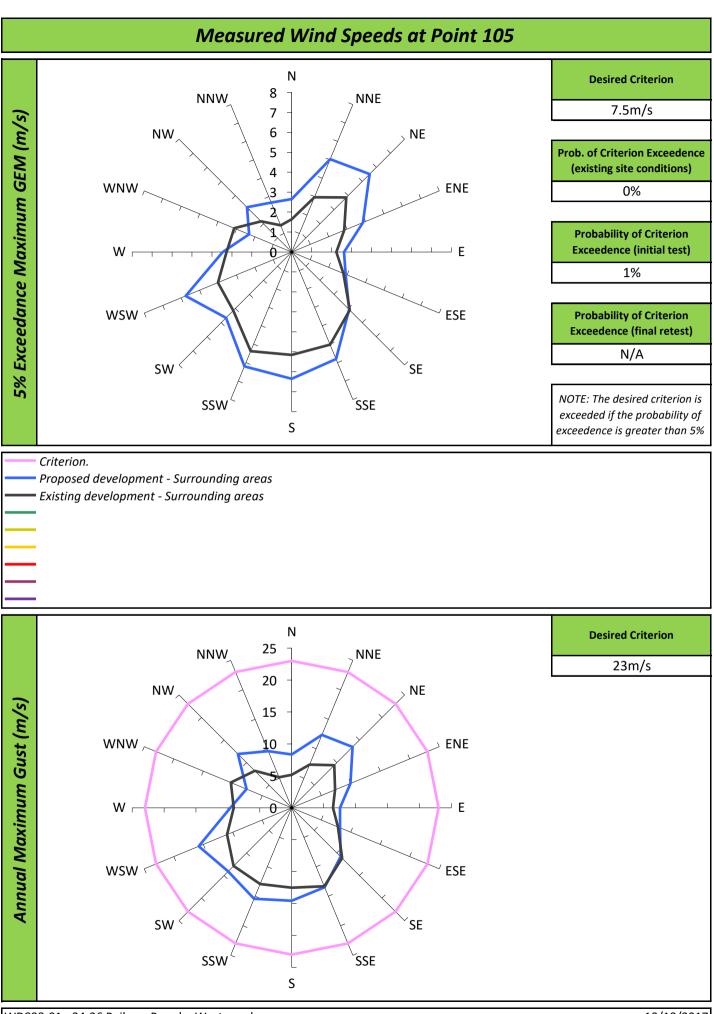




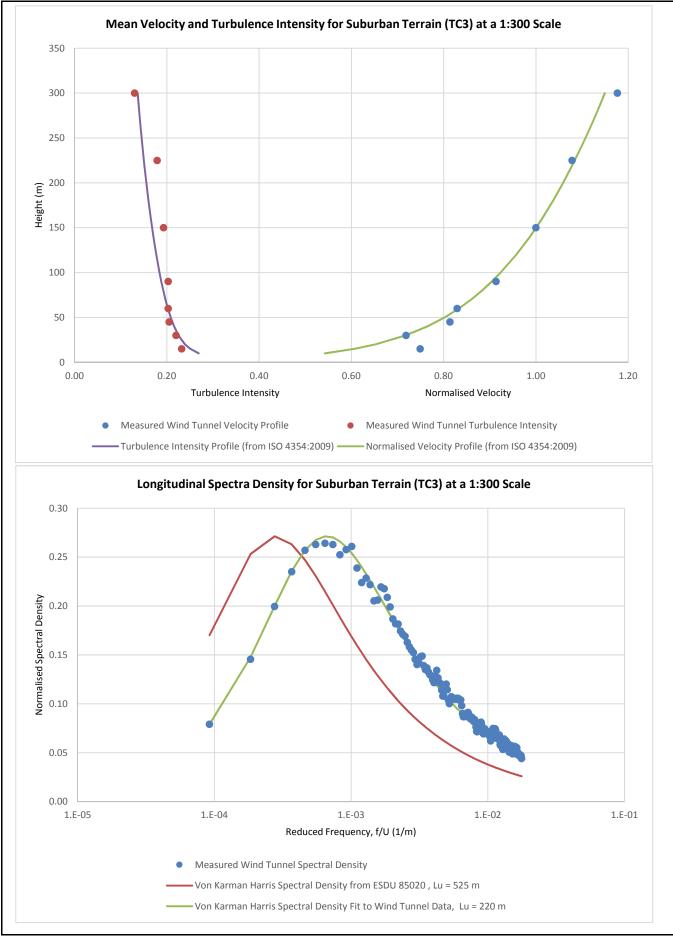








## **APPENDIX B - VELOCITY AND TURBULENCE INTENSITY PROFILES**



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